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采用还原方法的不确定关联时滞系统的鲁棒分散镇定

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摘 要: 针对一类具有多输入时滞项及互联时滞项的不确定关联系统, 提出了系统可鲁棒分散镇定的充分条件, 即一组线性矩阵不等式(LM I)有解. 系统的不确定性是未知时变且范数有界的, 基于还原方法及 LM I 技术给出系统设计状态反馈分散控制器的方法. 该控制器保证闭环系统全局渐近稳定, 且设计简单, 计算量小, 易于工程实现. 最后通过仿真例子说明了该方法的有效性.

关键词: 不确定关联时滞系统; 鲁棒分散镇定; 还原方法; 线性矩阵不等式

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Robust decentralized stabilization for uncertain interconnected delayed systems using reduction method

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Abstract: The problem of the robust stabilization for a class of uncertain interconnected systems with time delays in the input and interconnection is investigated. The uncertainties are time-varying and norm bounded. Based on the reduction method, a decentralized feedback controller is proposed such that the closed loop system is global asymptotically stable, and a sufficient condition for the stability is derived in terms of a linear matrix inequality (LM I). The design approach is simple. Simulation example shows the effectiveness of the proposed method.

Key words: uncertain interconnected delayed systems; robust decentralized stabilization; reduction method; linear matrix inequalities

1 引 言

在实际控制系统中普遍存在时滞现象, 使系统产生振荡和不稳定. 又因为建模误差等原因, 系统还含有一些不确定因素. 对此, 目前已取得了许多研究成果^[1-5], 如文献[1, 2]的 Riccati 方程方法; [3, 4]的线性矩阵不等式的设计方法; [5]提出的一种处理控制输入时滞的还原方法. 上述文献讨论的是集中控制问题. 近年来, 关联时滞系统的分散镇定问题也受到了学者们的关注^[6-9], 所设计的分散无记忆状

态反馈控制器保证了闭环系统的稳定性. 但利用还原方法处理不确定关联时滞系统的分散镇定问题, 研究结果还非常少见.

本文将还原方法扩展到大系统, 研究了一类具有参数不确定性的关联时滞大系统的鲁棒分散镇定问题. 系统不仅含有多重输入时滞, 而且互联项中也存在时滞. 文中采用还原方法, 并结合线性矩阵不等式技术, 给出了经状态变换后的系统渐近稳定的充分条件, 其结果由 N 个线性不等式给出, 并设计了

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分散控制器 这种设计方法的优点在于无需关注系统不确定参数的变化就能有效地计算出控制增益, 并且在系统的时滞大小信息可用时, 所给出的系统可分散镇定的条件具有相对较小的保守性, 适用范围较广.

2 系统描述及预备知识

考虑由以下 N 个关联子系统 $S_i (i = 1, 2, \dots, N)$ 组成的不确定时滞大系统:

$$S_i = \begin{cases} \dot{x}_i(t) = (A_i + \Delta A_i(t))x_i(t) + \sum_{p=0}^r B_{ip}u_i(t - h_{ip}) + \sum_{q=0}^s \Delta B_{iq}(t)u_i(t - \tau_{iq}) + \sum_{j=1, j \neq i}^N A_{ij}x_j(t - d_i), \\ x_i(t) = \Phi_i(t), u_i(t) = \Psi_i(t), t \in [-T_i, 0] \end{cases} \quad (1)$$

其中: $x_i \in R^{n_i}$ 和 $u_i \in R^{m_i}$ 分别为第 i 个子系统的状态向量和控制输入向量; $A_i, B_{ip} (p = 0, 1, \dots, r)$ 和 A_{ij} 为具有适当维数的已知实值常数矩阵; $\Delta A_i(t)$ 和 $\Delta B_{iq}(t) (q = 0, 1, \dots, s)$ 为时变不确定矩阵; $h_{ip} (p = 0, 1, \dots, r)$ 为已知时滞常数, 且 $h_{i0} = 0$; $\tau_{iq} (q = 0, 1, \dots, s)$ 为不确定输入项中未知时滞; d_i 为关联项中的未知正常数时滞; $T_i = \max\{h_{ip}, \tau_{iq}, d_i\}$; $\Phi_i(t)$ 为连续的状态向量初值函数

假设系统 (1) 的参数不确定性具有如下形式:

$$\Delta A_i(t) = D_i F_i(t) E_i, \Delta B_{iq}(t) = M_{iq} F_{iq}(t) N_{iq}, \quad i = 1, 2, \dots, N, q = 0, 1, \dots, s \quad (2)$$

其中: D_i, E_i, M_{iq} 和 N_{iq} 为相应维数的已知常数矩阵; $F_i(t)$ 和 $F_{iq}(t)$ 为满足

$$F_i^T(t) F_i(t) \leq I, F_{iq}^T(t) F_{iq}(t) \leq I \quad (3)$$

的未知矩阵函数, 且 $F_i(t)$ 和 $F_{iq}(t)$ 的各元素 Lebesgue 可测

采用还原方法, 考虑如下线性变换:

$$z_i(t) = x_i(t) + \sum_{p=0}^r \int_{t-h_{ip}}^t e^{A_i(t-\alpha_p-h_{ip})} B_{ip} u_i(\alpha_p) d\alpha_p, \quad (4)$$

则系统 (1) 可转换成

$$\dot{z}_i(t) = (A_i + D_i F_i(t) E_i) z_i(t) + \sum_{p=0}^r e^{-A_i h_{ip}} B_{ip} u_i(t) + \sum_{q=0}^s M_{iq} F_{iq}(t) N_{iq} u_i(t - \tau_{iq}) + \sum_{j=1, j \neq i}^N A_{ij} z_j(t - d_i) - \sum_{p=0}^r \int_{t-h_{ip}}^t D_i F_i(t) E_i e^{A_i(t-\alpha_p-h_{ip})} B_{ip} u_i(\alpha_p) d\alpha_p$$

$$\sum_{j=1, j \neq i}^N \sum_{p=0}^r \int_{t-d_i-h_{jp}}^{t-d_i} A_{ij} e^{A_j(t-d_i-\alpha_p-h_{jp})} B_{jp} u_j(\alpha_p) d\alpha_p \quad (5)$$

从式 (5) 可以看出, 由于存在不确定项及互联项, 系统 (1) 并没有完全还原成一个无时滞系统 本文的目的是对系统 (5) 设计鲁棒分散稳定控制器

$$u_i(t) = K_i z_i(t), \quad (6)$$

其中 $K_i \in R^{m_i \times n_i}$ 为增益矩阵, 使得如下闭环系统渐近稳定:

$$\dot{z}_i = (A_i + D_i F_i(t) E_i) z_i + \sum_{p=0}^r e^{-A_i h_{ip}} B_{ip} K_i z_i + \sum_{q=0}^s M_{iq} F_{iq}(t) N_{iq} K_i z_i(t - \tau_{iq}) + \sum_{j=1, j \neq i}^N A_{ij} z_j(t - d_i) - \sum_{p=0}^r \int_{t-h_{ip}}^t D_i F_i(t) E_i e^{A_i(t-\alpha_p-h_{ip})} B_{ip} K_i z_i(\alpha_p) d\alpha_p - \sum_{j=1, j \neq i}^N \sum_{p=0}^r \int_{t-d_i-h_{jp}}^{t-d_i} A_{ij} e^{A_j(t-d_i-\alpha_p-h_{jp})} B_{jp} K_j z_j(\alpha_p) d\alpha_p \quad (7)$$

3 分散鲁棒镇定

在推导主要结果之前, 首先给出下列引理

引理 1 对任何适当维数的实向量 X, Y 及正数 $\epsilon > 0$, 有下列不等式成立:

$$X Y + Y^T X^T - \epsilon X^T + \epsilon^{-1} Y^T Y. \quad (8)$$

引理 2 线性矩阵不等式

$$\begin{bmatrix} H(x) & S(x) \\ S(x)^T & R(x) \end{bmatrix} > 0$$

等价于

$$R(x) > 0, H(x) - S(x) R(x)^{-1} S(x)^T > 0$$

其中: $H(x) = H(x)^T, R(x) = R(x)^T$.

定理 1 若存在对称正定矩阵 $X_i \in R^{n_i \times n_i}$, 矩阵 $Y_i \in R^{m_i \times n_i}$ 及正常数 $\epsilon, \sigma_{iq}, \delta_{ip} (p = 0, 1, \dots, r; q = 0, 1, \dots, s; i = 1, 2, \dots, N)$, 使得如下的线性矩阵不等式成立:

$$\begin{bmatrix} \bar{A}_i & X_i E_i^T & Z_{i1} & Z_{i2} & Z_{i2} & X_i \\ E_i X_i & -\epsilon I & 0 & 0 & 0 & 0 \\ Z_{i1}^T & 0 & -\Lambda_{i1} & 0 & 0 & 0 \\ Z_{i2}^T & 0 & 0 & -\Lambda_{i2} & 0 & 0 \\ Z_{i2}^T & 0 & 0 & 0 & -\Lambda_{i3} & 0 \\ X_i & 0 & 0 & 0 & 0 & \frac{I}{1-N} \end{bmatrix} < 0, \quad (9)$$

则系统(5)可由分散状态反馈控制器(6)鲁棒镇定,并使闭环系统全局渐近稳定.式(9)中

$$\begin{aligned} \bar{A}_i = & A_i X_i + X_i A_i^T + \int_{p=0}^r e^{-A_i h_{ip}} B_{ip} Y_i + \\ & Y_i^T \left(\int_{p=0}^r e^{-A_i h_{ip}} B_{ip} \right)^T + (1+r) \sum_{j=1, j \neq i}^N A_{ij} A_{ij}^T + \\ & \left(\epsilon_i + \int_{p=0}^r \delta_{ip} \right) D_i D_i^T + \sum_{q=0}^s \sigma_{iq} M_{iq} M_{iq}^T, \\ Z_{i1} = & [Y_i^T N_{i0}^T, Y_i^T N_{i1}^T, \dots, Y_i^T N_{is}^T], \\ Z_{i2} = & [Y_i^T B_{i1}^T, Y_i^T B_{i2}^T, \dots, Y_i^T B_{ir}^T], \\ \Lambda_{i1} = & \text{diag} \{ \sigma_{i0} I, \sigma_{i1} I, \dots, \sigma_{is} I \}, \\ \Lambda_{i2} = & \text{diag} \{ \delta_{i1} G_{i1}, \delta_{i2} G_{i2}, \dots, \delta_{ir} G_{ir} \}, \\ \Lambda_{i3} = & \text{diag} \left\{ \frac{1}{N-1} H_{i1}, \dots, \frac{1}{N-1} H_{ir} \right\}. \end{aligned}$$

证明 选取Lyapunov函数如下:

$$V = \sum_{i=1}^N (V_{i1} + V_{i2} + V_{i3} + V_{i4} + V_{i5}). \quad (10)$$

其中

$$\begin{aligned} V_{i1} = & z_i^T(t) P_i z_i(t), \\ V_{i2} = & \int_{q=0}^s \int_{t-h_{iq}}^t z_i^T(\alpha_{iq}) Q_{iq} z_i(\alpha_{iq}) d\alpha_{iq}, \\ V_{i3} = & \int_{p=0}^r \int_0^{h_{ip}-t} z_i^T(\alpha) K_{ip}^T B_{ip}^T e^{A_i(\beta_{ip}-h_{ip})} R_{ip} \times \\ & e^{A_i(\beta_{ip}-h_{ip})} B_{ip} K_{ip} z_i(\alpha) d\alpha d\beta_{ip}, \\ V_{i4} = & \sum_{j=1, j \neq i}^N \int_{t-d_i}^t z_j^T(\theta) z_j(\theta) d\theta, \\ V_{i5} = & \sum_{j=1, j \neq i}^N \int_{p=0}^r \int_0^{h_{jp}-t} z_j^T(\alpha) K_{jp}^T B_{jp}^T \times \\ & e^{A_j(\beta_{jp}-h_{jp})} S_{jp} e^{A_j(\beta_{jp}-h_{jp})} B_{jp} K_{jp} z_j(\alpha) d\alpha d\beta_{jp}, \end{aligned}$$

P_i 为对称正定阵,而正定阵 Q_{iq} 及非负定矩阵 R_{ip} 和 S_{jp} 将在后面给出. V_{i1} 关于时间 t 的导数为

$$\begin{aligned} \dot{V}_{i1} = & 2z_i^T P_i \left(A_i + D_i F_i(t) E_i + \int_{p=0}^r e^{-A_i h_{ip}} B_{ip} K_{ip} \right) z_i + \\ & 2z_i^T P_i \left(\sum_{q=0}^s M_{iq} F_{iq}(t) N_{iq} K_{iq} z_i(t-\tau_{iq}) + \right. \\ & \sum_{j=1, j \neq i}^N A_{ij} z_j(t-d_i) - \sum_{j=1, j \neq i}^N \sum_{p=0}^r A_{ij} \times \\ & \left. \int_{t-d_i}^{t-h_{jp}} e^{A_j(t-d_i-\alpha_{jp}-h_{jp})} B_{jp} K_{jp} z_j(\alpha_{jp}) d\alpha_{jp} - \right. \\ & \left. \int_{p=0}^r D_i F_i(t) E_i \int_{t-h_{ip}}^t e^{A_i(t-\alpha_p-h_{ip})} B_{ip} K_{ip} z_i(\alpha_p) d\alpha_p \right). \end{aligned} \quad (11)$$

应用引理1及不等式^[5]

$$\int_{t-h}^t x^T(\alpha) d\alpha \int_{t-h}^t x(\alpha) d\alpha \geq \int_{t-h}^t x^T(\alpha) x(\alpha) d\alpha \quad (12)$$

可得

$$\begin{aligned} \dot{V}_{i1} = & z_i^T \left(P A_i + A_i^T P_i + \int_{p=0}^r e^{-A_i h_{ip}} B_{ip} K_{ip} + \right. \\ & K_{ip}^T \left(\int_{p=0}^r e^{-A_i h_{ip}} B_{ip} \right)^T P_i + \sum_{j=1, j \neq i}^N (1+r) P A_{ij} A_{ij}^T P_i + \\ & \left. \left(\epsilon_i + \int_{p=0}^r \delta_{ip} \right) P D_i D_i^T P_i + \epsilon_i^T E_i E_i + \right. \\ & \left. \sum_{q=0}^s \sigma_{iq} P M_{iq} M_{iq}^T P_i \right) z_i + \\ & \sum_{j=1, j \neq i}^N z_j^T(t-d_i) z_j(t-d_i) + \\ & \sum_{q=0}^s \bar{\sigma}_{iq}^T z_i^T(t-\tau_{iq}) K_{iq}^T N_{iq}^T N_{iq} K_{iq} z_i(t-\tau_{iq}) + \\ & \int_{p=0}^r \int_{t-h_{ip}}^t \delta_{ip}^T h_{ip} z_i^T(\alpha_{ip}) K_{ip}^T B_{ip}^T e^{A_i(t-\alpha_{ip}-h_{ip})} E_i^T \times \\ & E_i e^{A_i(t-\alpha_{ip}-h_{ip})} B_{ip} K_{ip} z_i(\alpha_{ip}) d\alpha_{ip} + \\ & \sum_{j=1, j \neq i}^N \int_{p=0}^r \int_{t-d_i-h_{jp}}^{t-d_i} h_{jp} z_j^T(\alpha_{jp}) K_{jp}^T B_{jp}^T e^{A_j(t-d_i-\alpha_{jp}-h_{jp})} \times \\ & e^{A_j(t-d_i-\alpha_{jp}-h_{jp})} B_{jp} K_{jp} z_j(\alpha_{jp}) d\alpha_{jp}. \end{aligned} \quad (13)$$

而 $\dot{V}_{i2}, \dot{V}_{i3}, \dot{V}_{i4}$ 和 \dot{V}_{i5} 由下列关系式给出:

$$\begin{aligned} \dot{V}_{i2} = & \sum_{q=0}^s z_i^T Q_{iq} z_i - \sum_{q=0}^s z_i^T(t-\tau_{iq}) Q_{iq} z_i(t-\tau_{iq}), \quad (14) \\ \dot{V}_{i3} = & \int_{p=0}^r z_i^T K_{ip}^T B_{ip}^T \left[\int_0^{h_{ip}-t} e^{A_i^T(\beta_{ip}-h_{ip})} R_{ip} e^{A_i(\beta_{ip}-h_{ip})} d\beta_{ip} \right] \times \\ & B_{ip} K_{ip} z_i - \int_{p=0}^r \int_{t-h_{ip}}^t z_i^T(\alpha_{ip}) K_{ip}^T B_{ip}^T e^{A_i(t-\alpha_{ip}-h_{ip})} \times \\ & R_{ip} e^{A_i(t-\alpha_{ip}-h_{ip})} B_{ip} K_{ip} z_i(\alpha_{ip}) d\alpha_{ip}, \quad (15) \\ \dot{V}_{i4} = & \sum_{j=1, j \neq i}^N z_j^T z_j - \sum_{j=1, j \neq i}^N z_j^T(t-d_i) z_j(t-d_i), \quad (16) \\ \dot{V}_{i5} = & \sum_{j=1, j \neq i}^N \sum_{p=0}^r z_j^T K_{jp}^T B_{jp}^T \times \\ & \left[\int_0^{h_{jp}-t} e^{A_j^T(\beta_{jp}-h_{jp})} S_{jp} e^{A_j(\beta_{jp}-h_{jp})} d\beta_{jp} \right] B_{jp} K_{jp} z_j - \\ & \sum_{j=1, j \neq i}^N \sum_{p=0}^r \int_{t-d_i-h_{jp}}^{t-d_i} z_j^T(\alpha_{jp}) K_{jp}^T B_{jp}^T e^{A_j(t-\alpha_{jp}-d_i-h_{jp})} \times \end{aligned}$$

$$S_{jp} e^{A_j(t-\alpha_{jp}-d_i-h_{jp})} B_{jp} K_{jz_j}(\alpha_{jp}) d\alpha_{jp} \quad (17)$$

矩阵 Q_{iq} , R_{ip} 和 S_{jp} 取为

$$Q_{iq} = \bar{\sigma}_{iq}^{-1} K_i^T N_{iq}^T N_{iq} K_i, R_{ip} = \delta_{ip}^{-1} h_{ip} E_i^T E_i, \quad (18)$$

$$S_{jp} = h_{jp} I,$$

可得

$$V^\circ = \sum_{i=1}^N (V_{i1}^\circ + V_{i2}^\circ + V_{i3}^\circ + V_{i4}^\circ + V_{i5}^\circ)$$

$$= \sum_{i=1}^N \left(z_i^T \left[P A_i + A_i^T P_i + P_i \int_{p=0}^r e^{-A_i h_{ip}} B_{ip} K_i + K_i^T \int_{p=0}^r e^{-A_i h_{ip}} B_{ip} \right]^T P_i + \left(\epsilon_i + \int_{p=0}^r \delta_{ip} \right) P D_i^T P_i + \epsilon_i^{-1} E_i^T E_i + (1+r) \sum_{j=1, j \neq i}^N P A_{ij} A_{ij}^T P_i + (N-1) I + \sum_{q=0}^s \sigma_{iq} P M_{iq} M_{iq}^T P_i + \sum_{q=0}^s \bar{\sigma}_{iq}^{-1} K_i^T N_{iq}^T N_{iq} K_i + \sum_{p=0}^r \delta_{ip}^{-1} K_i^T B_{ip}^T \int_{h_{ip}}^{h_{ip}+h_{ip}^0} e^{A_i^T (\beta_{ip}-h_{ip})} E_i^T E_i \times e^{A_i (\beta_{ip}-h_{ip})} d\beta_{ip} \right) B_{ip} K_i + \sum_{p=0}^r (N-1) K_i^T B_{ip}^T \times (h_{ip} \int_0^{h_{ip}} e^{A_i^T (\beta_{ip}-h_{ip})} e^{A_i (\beta_{ip}-h_{ip})} d\beta_{ip}) B_{ip} K_i | z_i \rangle, \quad (19)$$

即

$$V^\circ = \sum_{i=1}^N z_i^T W_i(\bullet) z_i = \sum_{i=1}^N z_i^T P_i X W_i(\bullet) X_i P_i z_i \quad (20)$$

其中

$$X_i = P_i^{-1}, \quad (21)$$

若矩阵 $X W_i(\bullet) X_i$ 是负定的, V° 必为负, 因此系统 (5) 是渐近稳定的

选取满足下式的正定矩阵 G_{ip} 和 H_{ip} :

$$G_{ip}^{-1} = \int_{h_{ip}}^0 e^{A_i^T \alpha_{ip}} E_i^T E_i e^{A_i \alpha_{ip}} d\alpha_{ip},$$

$$H_{ip}^{-1} = \int_{h_{ip}}^0 e^{A_i^T \alpha_{ip}} e^{A_i \alpha_{ip}} d\alpha_{ip}, \quad (22)$$

利用引理 2 (Schur 补), 并作变量变换 $Y_i = K X_i$, 可直接得出不等式 $X W_i(\bullet) X_i < 0$ 等价于 LM I(9). 由此定理 1 结论得证

注 1 由于分散稳定控制器 (6) 作用于还原的系统 (5) 后, 得到的闭环系统是渐近稳定的, 即当 $t \rightarrow \infty$ 时, $z_i(t)$ 和 $u_i(t)$ 均趋于零, 因此 $x_i(t)$ 也趋于零. 这表明原系统 (1) 也是渐近稳定的

注 2 定理 1 采用线性矩阵不等式的形式给出了不确定关联时滞系统鲁棒分散镇定的充分条件.

利用 Matlab 的工具箱 LM ITool, 可方便地解出式 (9) 中的 X_i 和 Y_i , 进而可求得分散控制器增益为 $K_i = Y_i X_i^{-1}$. 与文献 [8] 中基于 Riccati 方程的结果相比, LM I 在 LM ITool 的环境下, 求解非常方便, 不需要预先对多个参数和正定矩阵进行调整, 因而更具有数值易解性

注 3 与文献 [9] 中设计的分散无记忆状态反馈控制器方案相比, 在系统的控制输入项时滞信息可用时, 尤其是当时滞很小时, 本文给出的系统可分散镇定的条件具有相对较小的保守性, 且适用范围较广.

4 仿真实例

考虑由以下两个子系统组合而成的不确定关联时滞系统:

$$\dot{x}_1 = \left[\begin{array}{cc} 0 & 1 \\ 0 & 2 \end{array} \right] x_1 + \left[\begin{array}{cc} 0 & 0.4 \cos t \\ 0.2 \sin t & 0 \end{array} \right] u_1 + \left[\begin{array}{c} 0 \\ 1 \end{array} \right] u_1(t-h_{11}) + \left[\begin{array}{c} 0 \\ 0.1 \sin t \end{array} \right] u_1(t-\tau_{10}) + \left[\begin{array}{cc} 0.1 \cos t & 0 \\ 0 & 0 \end{array} \right] u_1(t-\tau_{11}) + \left[\begin{array}{cc} 0.05 & 0 \\ 0 & 0.15 \end{array} \right] x_2(t-d_1),$$

$$\dot{x}_2 = \left[\begin{array}{cc} -0.9 & 0.5 \\ 0 & 1 \end{array} \right] x_2 + \left[\begin{array}{cc} 0.1 \cos t & 0 \\ 0 & 0.2 \sin t \end{array} \right] u_2 + \left[\begin{array}{c} 1 \\ 1 \end{array} \right] u_2 + \left[\begin{array}{c} 1 \\ 1 \end{array} \right] u_2(t-h_{21}) + \left[\begin{array}{c} 0 \\ 0.05 \sin t \end{array} \right] u_2(t-\tau_{20}) + \left[\begin{array}{cc} 0.1 \cos t & 0 \\ 0 & 0 \end{array} \right] u_2(t-\tau_{21}) + \left[\begin{array}{cc} 0 & 0.05 \\ 0.02 & 0.1 \end{array} \right] x_1(t-d_2).$$

其中

$$h_{11} = \tau_{10} = \tau_{11} = 1, d_1 = 0.5, h_{21} = 0.8,$$

$$\tau_{20} = \tau_{21} = 0.5, d_2 = 0.3,$$

对此系统, 若应用文献 [9] 中得到的系统鲁棒镇定充分条件, 其 LM I 没有解, 设计方法失效, 将无法给出分散镇定控制器

采用本文提出的设计方法, 将系统与式 (2) 和 (3) 相比较, 可得

$$D_1 = \begin{bmatrix} 0.6325 & 0 \\ 0 & 0.4472 \end{bmatrix},$$

$$E_1 = \begin{bmatrix} 0 & 0.6325 \\ 0.4472 & 0 \end{bmatrix},$$

$$D_2 = \begin{bmatrix} 0.3162 & 0 \\ 0 & 0.4472 \end{bmatrix},$$

$$E_2 = \begin{bmatrix} 0 & 316 & 2 & 0 \\ 0 & 0 & 447 & 2 \end{bmatrix},$$

$$M_{10} = \begin{bmatrix} 0 \\ 0 & 316 & 2 \end{bmatrix}, M_{11} = \begin{bmatrix} 0 & 316 & 2 \\ 0 \end{bmatrix},$$

$$M_{20} = \begin{bmatrix} 0 \\ 0 & 223 & 6 \end{bmatrix}, M_{21} = \begin{bmatrix} 0 & 316 & 2 \\ 0 \end{bmatrix},$$

$$N_{10} = N_{11} = N_{21} = 0 \ 316 \ 2,$$

$$N_{20} = 0 \ 223 \ 6$$

根据式(22),取如下正定矩阵:

$$G_{11} = \begin{bmatrix} 5 & 798 & 0 & 2 & 810 & 0 \\ 2 & 810 & 0 & 9 & 894 & 3 \end{bmatrix},$$

$$H_{11} = \begin{bmatrix} 1 & 309 & 7 & 1 & 091 & 3 \\ 1 & 091 & 3 & 3 & 845 & 3 \end{bmatrix},$$

$$G_{21} = \begin{bmatrix} 7 & 239 & 9 & 2 & 341 & 4 \\ 2 & 341 & 4 & 15 & 583 & 7 \end{bmatrix},$$

$$H_{21} = \begin{bmatrix} 0 & 425 & 2 & 0 & 395 & 3 \\ 0 & 395 & 3 & 2 & 273 & 2 \end{bmatrix}.$$

求解LM I(9),在LM ITooI环境下,可一次性解得

$$X_1 = \begin{bmatrix} 0 & 340 & 4 & - & 0 & 249 & 7 \\ - & 0 & 249 & 7 & 0 & 210 & 1 \end{bmatrix}, \epsilon_1 = 0 \ 331 \ 7,$$

$$\sigma_{10} = 1 \ 658 \ 5, \sigma_{11} = 0 \ 699 \ 8, \delta_{10} = 0 \ 044 \ 9,$$

$$\delta_{11} = 0 \ 327 \ 7, Y_1 = [0 \ 490 \ 1 \ - \ 1 \ 280 \ 6],$$

$$X_2 = \begin{bmatrix} 1 & 887 & 5 & 0 & 457 & 7 \\ 0 & 457 & 7 & 0 & 132 & 6 \end{bmatrix}, \epsilon_2 = 0 \ 395 \ 6,$$

$$\sigma_{20} = 0 \ 611 \ 4, \sigma_{21} = 1 \ 451 \ 5, \delta_{20} = 0 \ 075 \ 3,$$

$$\delta_{21} = 0 \ 271 \ 5, Y_2 = [- \ 1 \ 124 \ 1 \ - \ 0 \ 631 \ 1]$$

分散控制器为

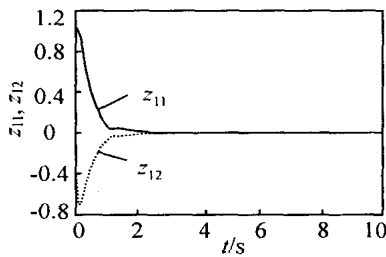


图1 闭环子系统1的状态轨迹

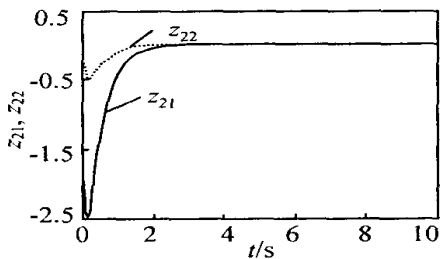


图2 闭环子系统2的状态轨迹

$$u_1(t) = [- \ 23 \ 612 \ 9 \ - \ 34 \ 155 \ 4]z_1(t),$$

$$u_2(t) = [3 \ 418 \ 0 \ - \ 16 \ 552 \ 4]z_2(t).$$

闭环子系统的状态响应曲线如图1和图2所示

5 结 语

对于具有时滞及参数不确定性的关联大系统的鲁棒分散镇定问题,本文采用还原方法,结合线性矩阵不等式给出了还原系统渐近稳定的充分条件,并设计了分散控制器.该方法无需经过任何参数调整的过程,解N个特定的LM I,便可得到分散镇定已知系统的控制器.仿真例子说明了该方法是有效的且简便易行.

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