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一类不确定非线性纯反馈系统的自适应鲁棒模糊控制

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摘要: 针对一类带有不确定性的非线性 MIMO 纯反馈系统, 提出一种自适应鲁棒模糊控制方法. 该方法放宽了已有文献对系统模型的限制条件, 基于李雅普诺夫分析方法获得了控制输入和自适应律. 在控制输入设计中, 鲁棒控制项用于补偿逼近误差向量. 通过选择适当的设计参数, 提出的控制方法使得闭环系统的所有信号是一致有界的和跟踪误差向量的范数收敛到小的零邻域内. 仿真结果表明了所提出方法的有效性.

关键词: 自适应模糊控制; 鲁棒控制; 非线性纯反馈系统; 不确定性; Backstepping

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Adaptive robust fuzzy control for a class of uncertain nonlinear pure-feedback systems

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Abstract: An adaptive robust fuzzy control approach is presented for a class of nonlinear MIMO pure-feedback systems with uncertainties. The restriction condition of the system model in the existing literatures is relaxed. The control inputs and the adaptation laws are obtained based on Lyapunov analysis approach. The robust control terms are utilized to compensate the approximation error vectors in the control input design. By choosing suitable design parameters, all the signals in the resulting closed-loop system are uniformly bounded and the norm of the tracking error vector converges to an arbitrarily small neighborhood around zero by using the presented control approach. Simulation results show the effectiveness of the presented approach.

Key words: Adaptive fuzzy control; Robust control; Nonlinear pure-feedback systems; Uncertainty; Backstepping

1 引言

在许多实际情况下, 非线性系统很难通过已知非线性函数精确地描述, 不确定性时时存在. 已经证明, 模糊逻辑系统或神经网络能一致逼近任意不确定非线性连续函数到任意精度. 在过去十几年里, 对于不确定系统的研究, 已经取得了许多有意义的成果^[1-10]. 利用模糊逻辑系统的逼近特性, 针对带有完全未知函数的非线性系统, 文献[1-3]提出了几种稳定的自适应控制算法, 所提出的算法可保证系统的所有信号是有界的, 并且实现了系统的 H 跟踪性能. 但是, 文献[1-3]提供的算法仅适用于匹配条件确定类型的非线性系统. 近十年, 对于三角结构的不确定非线性系统的研究, 已引起了研究者的兴

趣^[4-10]. Backstepping 方法对于解决三角结构的非线性系统的控制律设计问题是非常有效的^[4]. 文献[4, 9]对线性参数化不确定严格反馈和纯反馈系统设计了自适应 Backstepping 控制器. 然而, 在许多情况下不确定性是不能线性参数化或者是完全未知的. 文献[5-7]利用 Backstepping 方法针对 SISO 不确定非线性严格反馈系统提出了几种稳定的自适应控制方案. 文献[8]针对 MIMO 严格反馈系统提出了一个稳定的鲁棒自适应模糊控制设计算法. 文献[10]利用前馈神经网络的逼近特性, 针对带有完全未知函数的 SISO 纯反馈系统设计了稳定的自适应控制方法, 保证了系统信号是一致有界的.

考虑如下形式的多输入多输出纯反馈系统:

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$$\begin{cases} \dot{x}_i = F_i^0(\bar{x}_{i+1}) + F_i^*(\bar{x}_{i+1}) + G_i(\bar{x}_{i+1})x_{i+1}, \\ \dot{x}_n = F_n^0(x) + F_n^*(x) + G_n(x)u, \\ y = x_1, 1 \leq i \leq n-1. \end{cases} \quad (1)$$

其中: $x_i \in R^{n_i}$ 表示第 i 个子系统的状态, $x = \bar{x}_n = [x_1^T, \dots, x_n^T]^T$ 表示整个系统的状态, u 表示系统的控制输入, y 表示系统的输出, $\bar{x}_i = [x_1^T, \dots, x_i^T]^T$, $F_i^0(\bar{x}_{i+1})$ 和 $F_n^0(x)$ 是已知标称向量值函数, $F_i^*(\bar{x}_{i+1})$ 和 $F_n^*(x)$ 是未知向量值函数, $G_i(\bar{x}_i)$ 和 $G_n(x)$ 是已知的矩阵值函数且是行满秩的. 系统(1)与文献[9,10]中研究的系统模型相比较,不要求子系统的状态是标量,且系统(1)中的不确定性没有参数线性化的要求. 在文献[8]中,研究的系统模型为 $F_i(\bar{x}_{i+1}) = F_i(\bar{x}_i)$ 和 $G_i(\bar{x}_{i+1}) = G_i(\bar{x}_i)$, $i = 1, 2, \dots, n-1$, 即文献[8]中第 i 个子系统的不确定项不依赖于第 $i+1$ 个子系统的状态 x_{i+1} . 因此,本文提出的方法进一步放宽了对系统模型的限制条件.

2 问题描述

利用模糊逻辑系统的逼近特性,未知向量值函数 $F_i^*(\bar{x}_{i+1})$ ($i = 1, 2, \dots, n-1$) 和 $F_n^*(x)$ 可表示为

$$\begin{cases} F_i^*(\bar{x}_{i+1}) = B_i(\bar{x}_{i+1}) \hat{i}^* + \tilde{i}, \\ i = 1, 2, \dots, n-1; \\ F_n^*(x) = B_n(x) \hat{n}^* + \tilde{n}. \end{cases} \quad (2)$$

其中: B_i 表示基函数矩阵, \hat{i}^* 表示最优逼近参数向量, \tilde{i} 是最优逼近误差向量.

有界参考信号 $y_d(t) \in R^{n_1}$ 是一个给定的光滑向量值函数,控制的目的是对于系统(1)设计一个模糊控制器,能实现闭环系统的所有信号是一致有界的,并且跟踪误差向量 $z_1 = x_1 - y_d(t)$ 的 2-范数收敛到任意指定小的零邻域内.

3 自适应鲁棒模糊控制器设计

在下面的自适应模糊控制设计的推导中,模糊系统的逼近特性只在某一紧集内成立. 因此,本文得到的稳定性结果是半全局意义下的. 令 $u = x_{(n+1)d}$, $z_{n+1} = 0$,设计过程如下:

Step1 为了符号上的统一,令 $x_{1d} = y_d(t)$, 定义跟踪误差向量 $z_1 = x_1 - x_{1d}$, z_1 的导数为

$$\dot{z}_1 = F_1^0(\bar{x}_2) + F_1^*(\bar{x}_2) + G_1(\bar{x}_2)z_2 - \dot{x}_{1d}. \quad (3)$$

对最优逼近误差向量 \tilde{i} 作如下假设:

假设 1 对每一个 $i = 1, 2, \dots, n$, 最优逼近误差向量 \tilde{i} 满足 $\|\tilde{i}\| \leq \hat{i}^*$, 其中 $\hat{i}^* > 0$ 是未知常数.

遍及本文,利用 \hat{i} 和 \tilde{i} 分别表示 \hat{i}^* , \tilde{i}^* 的估计值以及定义 $\tilde{i} = \hat{i} - \tilde{i}^*$, $\tilde{i} = \hat{i} - \tilde{i}^*$, 用符号 $\|\cdot\|$ 表示 2-范数. 选择虚拟控制输入向量

$$x_{2d} = -G_1^+ [k_1 z_1 + F_1^0(\bar{x}_2) +$$

$$B_1(\bar{x}_2) \hat{1}^* - \dot{x}_{1d}]. \quad (4)$$

其中: $G_1^+ = G_1^T [G_1 G_1^T]^{-1}$ 表示 G_1 的 Moore-Penrose 广义逆, $\hat{1}^* = \frac{\Lambda_1^2}{\Lambda_1 z_1^T z_1 + 1}$ 和 $\tilde{1}^*$ 是正的设计常数.

引入向量 $z_2 = x_2 - x_{2d}$, 将式(2), (4) 代入式(3), 可得

$$\dot{z}_1 = -k_1 z_1 + G_1 z_2 - B_1(\bar{x}_2) \tilde{1} + \tilde{1} + \dot{x}_{1d}. \quad (5)$$

选择下面的李雅普诺夫函数:

$$V_1 = \frac{1}{2} z_1^T z_1 + \frac{1}{2} \tilde{1}^T \tilde{1} + \frac{1}{2} \tilde{1}^2. \quad (6)$$

其中: $\tilde{1}^T$ 是正定的增益矩阵, $\tilde{1}$ 是正的设计常数. V_1 沿着方程(5)的时间导数为

$$\begin{aligned} \dot{V}_1 = & z_1^T G_1 z_2 - k_1 z_1^T z_1 + \tilde{1}^T \tilde{1} [\hat{1} - \tilde{1} B_1^T(\bar{x}_2) z_1] + \\ & (\tilde{1}^T \tilde{1} + \tilde{1} z_1^T z_1 + \frac{1}{2} \tilde{1}^2). \end{aligned} \quad (7)$$

选择下列自适应律:

$$\dot{\hat{1}} = \tilde{1} [B_1^T(\bar{x}_2) z_1 - \tilde{1} \hat{1}], \quad (8)$$

$$\dot{\tilde{1}} = \tilde{1} (z_1 - \mu_1 \hat{1}), \quad (9)$$

其中 $\tilde{1}, \mu_1$ 是正的设计常数.

利用式(8), 可得

$$\begin{aligned} \tilde{1}^T \tilde{1} [\hat{1} - \tilde{1} B_1^T(\bar{x}_2) z_1] = & -\tilde{1}^T \hat{1} = \\ & -\tilde{1}^T \tilde{1} - \tilde{1}^T \tilde{1}^* \\ & - \frac{1}{2} \tilde{1}^T \tilde{1} + \frac{1}{2} \tilde{1}^{*2}. \end{aligned} \quad (10)$$

利用方程(9)和假设 1, 可得

$$\begin{aligned} z_1^T \tilde{1} + \tilde{1} z_1^T z_1 + \frac{1}{2} \tilde{1}^2 & \\ \tilde{1}^* z_1 + \tilde{1} z_1^T z_1 + \frac{1}{2} \tilde{1}^2 & \\ \hat{1} z_1 - \frac{\Lambda_1^2 z_1^T z_1}{\Lambda_1 z_1^T z_1 + 1} + \tilde{1} (\frac{1}{2} \hat{1} - z_1) & \\ \tilde{1} - \mu_1 \tilde{1} \hat{1} = \tilde{1} - \mu_1 \tilde{1}^* - \mu_1 \tilde{1} \tilde{1}^* & \\ \tilde{1} - \frac{\mu_1}{2} \tilde{1}^2 + \frac{\mu_1}{2} \tilde{1}^* / \tilde{1}^2. & \end{aligned} \quad (11)$$

将式(10)和(11)代入(7), 则有

$$\begin{aligned} \dot{V}_1 & \\ z_1^T G_1 z_2 - k_1 z_1^T z_1 - \frac{1}{2} \tilde{1}^T \tilde{1} - & \\ \frac{\mu_1}{2} \tilde{1}^2 + \frac{1}{2} \tilde{1}^{*2} + \frac{\mu_1}{2} \tilde{1}^* / \tilde{1}^2 + 1. & \end{aligned} \quad (12)$$

Step i ($i = 2, 3, \dots, n$) 在这一步, 将设计虚拟控制输入 $x_{(i+1)d}$. 定义误差向量 $z_i = x_i - x_{id}$, x_{id} 在

第 $i - 1$ 步已经得到且 x_{id} 的时间导数为

$$\dot{x}_{id} = \sum_{j=1}^i \frac{\partial x_{id}}{\partial x_j^T} \dot{x}_j - \dot{i}_{i-1}, \quad (13)$$

其中

$$\dot{i}_{i-1} = \sum_{j=1}^{i-1} \frac{\partial x_{id}}{\partial \hat{\Lambda}_j^T} \dot{\Lambda}_j + \sum_{j=1}^{i-1} \frac{\partial x_{id}}{\partial \Lambda_j} \dot{\Lambda}_j + \sum_{j=1}^i \frac{\partial x_{id}}{\partial y_d^{(j-1)T}} \dot{y}_d^{(j)}.$$

z_i 的导数为

$$\dot{z}_i = F_i^0(\bar{x}_{i+1}) + F_i^*(\bar{x}_{i+1}) + G_i(\bar{x}_{i+1})x_{i+1} - \dot{x}_{id}. \quad (14)$$

利用式(13)和(14),可得

$$\dot{z}_i = (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T}) \dot{x}_i - \sum_{j=1}^{i-1} \frac{\partial x_{id}}{\partial x_j^T} \dot{x}_j - \dot{i}_{i-1}, \quad (15)$$

其中定义 $I_j = I_{n_{j+1} \times n_{j+1}}$ ($j = 0, 1, \dots, n - 1$) 表示 $n_{j+1} \times n_{j+1}$ 的单位阵. 作如下假设:

假设2 对每个 $i = 1, 2, \dots, n - 1, n_{i+1} \times n_{i+1}$ 的矩阵 $(I_i - \frac{\partial x_{(i+1)d}}{\partial x_{i+1}^T})$ 是可逆的, $x_{(i+1)d}$ ($i = 1, 2, \dots, n$) 稍后定义.

考虑下面的李雅普诺夫函数:

$$V_i = V_{i-1} + \frac{1}{2} z_i^T z_i + \frac{1}{2} \tilde{\Lambda}_i^T \tilde{\Lambda}_i + \frac{1}{2} \tilde{\Lambda}_i^2. \quad (16)$$

其中: $\tilde{\Lambda}_i = \tilde{\Lambda}_i^T$ 是自适应增益正定矩阵, $\tilde{\Lambda}_i$ 是一个正的设计常数. V_i 沿着式(15)的时间导数为

$$\dot{V}_i = \dot{V}_{i-1} + z_i^T [(I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T}) \dot{x}_i - \sum_{j=1}^{i-1} \frac{\partial x_{id}}{\partial x_j^T} \dot{x}_j - \dot{i}_{i-1}] + \tilde{\Lambda}_i^T \tilde{\Lambda}_i + \frac{1}{\tilde{\Lambda}_i} \dot{\tilde{\Lambda}}_i. \quad (17)$$

结合式(1), (2) 和(17),可得

$$\begin{aligned} \dot{V}_i = & \dot{V}_{i-1} + z_i^T [(I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T}) [F_i^0(\bar{x}_{i+1}) + \\ & B_i(\bar{x}_{i+1}) \Lambda_i - i(I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^T z_i + G_i(\bar{x}_{i+1})x_{i+1}] - \\ & \sum_{j=1}^{i-1} \frac{\partial x_{id}}{\partial x_j^T} [F_j^0(\bar{x}_{j+1}) + B_j(\bar{x}_{j+1}) \Lambda_j + \\ & G_j(\bar{x}_{j+1})x_{j+1}] - \dot{i}_{i-1}] + \\ & z_i^T \sum_{j=1}^{i-1} \frac{\partial x_{id}}{\partial x_j^T} [B_j(\bar{x}_{j+1}) \tilde{\Lambda}_j - \dot{\Lambda}_j] + \\ & [z_i^T (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^T i + i \times \\ & z_i^T (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^2 + \frac{1}{\tilde{\Lambda}_i} \dot{\tilde{\Lambda}}_i] + \\ & \tilde{\Lambda}_i^{-1} \tilde{\Lambda}_i [\hat{\Lambda}_i - i B_i^T(\bar{x}_{i+1}) (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^T z_i]. \end{aligned} \quad (18)$$

其中

$$\tilde{\Lambda}_i = \frac{\tilde{\Lambda}_2}{\tilde{\Lambda}_i z_i^T (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^T + i},$$

$\tilde{\Lambda}_i$ 是正的常数. 选择下面的自适应律:

$$\dot{\hat{\Lambda}}_i = -i [B_i^T(\bar{x}_{i+1}) (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^T z_i - \tilde{\Lambda}_i \hat{\Lambda}_i], \quad (19)$$

$$\dot{\hat{\Lambda}}_i = -i [z_i^T (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T}) - \mu_i \hat{\Lambda}_i], \quad (20)$$

其中 $\tilde{\Lambda}_i, \mu_i$ 是正的设计常数.

利用方程(19)和(20),类似于不等式(10)和(11)的推导过程,有

$$\begin{aligned} & \tilde{\Lambda}_i^{-1} \tilde{\Lambda}_i [\hat{\Lambda}_i - i B_i^T(\bar{x}_{i+1}) (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^T z_i] \\ & - \frac{i}{2} \tilde{\Lambda}_i \tilde{\Lambda}_i + \frac{i}{2} \tilde{\Lambda}_i^* \tilde{\Lambda}_i^2, \end{aligned} \quad (21)$$

$$\begin{aligned} & z_i^T (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^T i + i \times \\ & z_i^T (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^2 + \frac{1}{\tilde{\Lambda}_i} \dot{\tilde{\Lambda}}_i \\ & - \frac{\mu_i}{2} \tilde{\Lambda}_i + \frac{\mu_i}{2} / \tilde{\Lambda}_i^* / \tilde{\Lambda}_i^2, \end{aligned} \quad (22)$$

$$\begin{aligned} & z_i^T \sum_{j=1}^{i-1} \frac{\partial x_{id}}{\partial x_j^T} B_j(\bar{x}_{j+1}) \tilde{\Lambda}_j \\ & - \sum_{j=1}^{i-1} \frac{i}{2} \tilde{\Lambda}_j \tilde{\Lambda}_j + \sum_{j=1}^{i-1} (\frac{1}{2} \tilde{\Lambda}_j^{-1} z_i^T \times \\ & \frac{\partial x_{id}}{\partial x_j^T} B_j(\bar{x}_{j+1}) B_j^T(\bar{x}_{j+1}) \frac{\partial x_{id}}{\partial x_j^T} z_i), \\ & z_i^T \sum_{j=1}^{i-1} \frac{\partial x_{id}}{\partial x_j^T} \tilde{\Lambda}_j - \sum_{j=1}^{i-1} \tilde{\Lambda}_j^* z_i^T \frac{\partial x_{id}}{\partial x_j^T} \\ & - \sum_{j=1}^{i-1} \frac{\mu_j}{2} / \tilde{\Lambda}_j^* / \tilde{\Lambda}_j^2 + \sum_{j=1}^{i-1} \frac{1}{2\mu_j} z_i^T \frac{\partial x_{id}}{\partial x_j^T} \frac{\partial x_{id}}{\partial x_j^T} z_i, \end{aligned} \quad (23)$$

其中 $\tilde{\Lambda}_j^{-1}, \mu_j^{-1}$ 是正的常数, $j = 1, 2, \dots, i - 1, i = 2, 3, \dots, n$.

将式(21) ~ (24) 代入(18),可得

$$\begin{aligned} \dot{V}_i = & \dot{V}_{i-1} + z_i^T (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T}) [F_i^0(\bar{x}_{i+1}) + \\ & B_i(\bar{x}_{i+1}) \Lambda_i - i(I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^T z_i + \\ & G_i(\bar{x}_{i+1})x_{i+1}] + z_i^T H_{i-1} - \frac{i}{2} \tilde{\Lambda}_i \tilde{\Lambda}_i + \\ & \sum_{j=1}^{i-1} \frac{i}{2} \tilde{\Lambda}_j \tilde{\Lambda}_j + \frac{i}{2} \tilde{\Lambda}_i^* \tilde{\Lambda}_i^2 - \frac{\mu_i}{2} \tilde{\Lambda}_i + \\ & \sum_{j=1}^{i-1} \frac{\mu_j}{2} / \tilde{\Lambda}_j^* / \tilde{\Lambda}_j^2 + \frac{\mu_i}{2} / \tilde{\Lambda}_i^* / \tilde{\Lambda}_i^2 + i. \end{aligned} \quad (25)$$

其中

$$\begin{aligned} H_{i-1} = & \sum_{j=1}^{i-1} \frac{1}{2} \frac{\partial x_{id}}{\partial x_j^T} B_j(\bar{x}_{j+1}) B_j^T(\bar{x}_{j+1}) \frac{\partial x_{id}}{\partial x_j^T} z_i - \\ & \sum_{j=1}^{i-1} \frac{\partial x_{id}}{\partial x_j^T} [F_j^0(\bar{x}_{j+1}) + B_j(\bar{x}_{j+1}) \Lambda_j + \end{aligned}$$

$$G_j(\bar{x}_{j+1})x_{j+1} - \dots + \frac{1}{2\mu_j^{i-1}} \frac{\partial x_{id}}{\partial x_j^T} \frac{\partial x_{id}^T}{\partial x_j} z_i. \tag{26}$$

经过步骤 1, 2, ..., i - 1 的推导, H_{i-1} 是可计算的.

引入误差向量 $z_{i+1} = x_{i+1} - x^{(i+1)d}$ 和选择虚拟控制输入

$$\begin{aligned} x^{(i+1)d} = & -G_i^T \{ F_i^0(\bar{x}_{i+1}) + B_i(\bar{x}_{i+1}) \wedge_i - \\ & i(I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^T z_i + (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T})^{-1} [G_{i-1}^T(I_{i-2} - \\ & \frac{\partial x_{(i-1)d}}{\partial x_{i-1}^T})^T z_{i-1} + k_i z_i + H_{i-1}] \}. \end{aligned} \tag{27}$$

在步骤 i - 1, 已经得到

$$\begin{aligned} \dot{V}_{i-1} = & z_{i-1}^T (I_{i-2} - \frac{\partial x_{(i-1)d}}{\partial x_{i-1}^T}) G_{i-1}(\bar{x}_i) z_i - \sum_{j=1}^{i-1} k_j z_j^T z_j - \\ & \frac{i-1}{2} \sum_{i=1}^{i-1} \tilde{\mu}_i + \sum_{j=1}^{i-2} (\frac{i}{2} - \frac{i-2}{r=j} \frac{r}{2}) \sum_{j=1}^{i-1} \tilde{\mu}_j + \\ & \sum_{j=1}^{i-1} \frac{\mu_j}{2} \tilde{\mu}_j + \sum_{j=1}^{i-1} \frac{i}{2} j^*{}^2 + \sum_{j=1}^{i-1} \frac{\mu_j}{2} / j^*{}^2 + \\ & \sum_{j=1}^{i-2} \sum_{r=j}^{i-2} \frac{\mu_r}{2} / j^*{}^2 + \sum_{j=1}^{i-1} j. \end{aligned} \tag{28}$$

将式(27)和(28)代入(25), 可得

$$\begin{aligned} \dot{V}_i = & z_i^T (I_{i-1} - \frac{\partial x_{id}}{\partial x_i^T}) G_i(\bar{x}_{i+1}) z_{i+1} - \sum_{j=1}^i k_j z_j^T z_j - \\ & \frac{i}{2} \sum_{i=1}^{i-1} \tilde{\mu}_i - \sum_{j=1}^{i-1} (\frac{i}{2} - \frac{i-1}{r=j} \frac{r}{2}) \sum_{j=1}^{i-1} \tilde{\mu}_j - \\ & \sum_{j=1}^i \frac{\mu_j}{2} \tilde{\mu}_j + \sum_{j=1}^i \frac{i}{2} j^*{}^2 + \sum_{j=1}^i \frac{\mu_j}{2} / j^*{}^2 + \\ & \sum_{j=1}^{i-1} \sum_{r=j}^{i-1} \frac{\mu_r}{2} / j^*{}^2 + \sum_{j=1}^i j, \end{aligned} \tag{29}$$

其中选择 $\frac{r}{2}, r = j, \dots, i - 1$, 使得 $\frac{i}{2} - \frac{r}{2} > 0, j = 1, 2, \dots, i - 1$.

在第 n 步中可得实际控制输入

$$\begin{aligned} u = x^{(n+1)d} = & -G_n^T \{ F_n^0(x) + B_n(x) \wedge_n - n(I_{n-1} - \\ & \frac{\partial x_{nd}}{\partial x_n^T})^T z_n + (I_{n-1} - \frac{\partial x_{nd}}{\partial x_n^T})^{-1} [G_{n-1}^T(I_{n-2} - \\ & \frac{\partial x_{(n-1)d}}{\partial x_{n-1}^T})^T z_{n-1} + k_n z_n + H_{n-1}] \}. \end{aligned} \tag{30}$$

在式(16)中, 当 $i = n$ 时, 有

$$\begin{aligned} V_n = & \frac{1}{2} \sum_{j=1}^n z_j^T z_j + \frac{1}{2} \sum_{j=1}^n \tilde{\mu}_j + \sum_{j=1}^n \frac{1}{2} \tilde{\mu}_j. \end{aligned} \tag{31}$$

在式(29)中, 当 $i = n$ 时, 有

$$\begin{aligned} \dot{V}_n = & - \sum_{j=1}^n k_j z_j^T z_j - \frac{n}{2} \sum_{n=1}^n \tilde{\mu}_n - \sum_{j=1}^{n-1} (\frac{n}{2} - \\ & \sum_{r=j}^{n-1} \frac{r}{2}) \sum_{j=1}^{n-1} \tilde{\mu}_j + \sum_{j=1}^n \frac{\mu_j}{2} \tilde{\mu}_j + \\ & \sum_{j=1}^n \frac{n}{2} j^*{}^2 + \sum_{j=1}^n \frac{\mu_j}{2} / j^*{}^2 + \\ & \sum_{j=1}^{n-1} \sum_{r=j}^{n-1} \frac{\mu_r}{2} / j^*{}^2. \end{aligned} \tag{32}$$

定理 1 考虑由方程(1)描述的系统, 给定有界参考信号 $y_d \in R^{n_1}$ 是一个充分光滑的向量值函数且 $\dot{y}_d, y_d^{(2)}, \dots, y_d^{(n)}$ 是有界的. 在假设 1 和假设 2 成立的条件下, 选择虚拟控制输入(4), (27)和实际控制输入(30), 选择自适应律(8), (9), (19)和(20). 假设存在充分大的紧集 $\Omega \subset R^{n_1+n_2+\dots+n_i} (i = 1, 2, \dots, n)$ 满足 $\bar{x}_i \in \Omega_i$. 那么, 所提出的控制方法可保证: 1) 闭环系统的所有信号是有界的; 2) 输出跟踪误差向量 z_1 的范数收敛到小的零邻域内.

证明 不等式(32)可以重新写成

$$\dot{V}_n \leq -V_n + \dots \tag{33}$$

其中

$$\begin{aligned} = & \sum_{j=1}^n \frac{n}{2} j^*{}^2 + \sum_{j=1}^n \frac{\mu_j}{2} / j^*{}^2 + \\ & \sum_{j=1}^{n-1} \sum_{r=j}^{n-1} \frac{\mu_r}{2} / j^*{}^2 + \sum_{j=1}^n j, \\ = & \min\{k^*, \mu^*\}, \\ k^* = & \min_j \{2k_j\}, \mu^* = \min_j \{\mu_j\}, \\ \mu^* = & \min_j \{ \min_{n-1} (n), (j - \sum_{r=j}^{n-1} r) \min(n-j) \}, \end{aligned}$$

$\min(n-j) (j = 1, \dots, n)$ 表示 j 的最小特征值.

解不等式(33), 得到

$$0 \leq V_n(t) \leq [V_n(0) + \dots] \exp(-t), \tag{34}$$

不等式(34)意味着 $V_n(t)$ 最终收敛到 \dots . 因此, 从式(31)和(34)中可以看出闭环系统的所有信号 $z_j, \tilde{\mu}_j, \mu_j, j = 1, 2, \dots, n$, 是一致有界的.

联合方程(31)和不等式(34), 得到

$$\frac{1}{2} \sum_{j=1}^n z_j^T z_j \leq [V_n(0) + \dots] \exp(-t). \tag{35}$$

式(35)意味着

$$\|z_1\|^2 \leq \sum_{j=1}^n z_j^T z_j \leq 2[V_n(0) + \dots] \exp(-t). \tag{36}$$

根据式(36), 给定 $\epsilon > \sqrt{2} / \gamma$, 存在 T , 对所有的 $t > T$, 跟踪误差向量 z_1 满足

$$\|z_1\| = \|x_1 - x_{1d}\| = \|y - y_d\| < \epsilon.$$

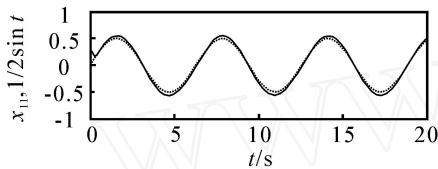
综上, 定理 1 成立.

4 仿真例子

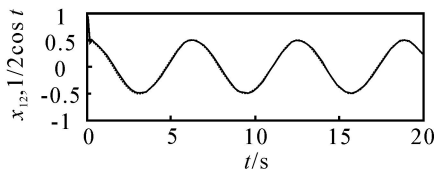
考虑如下的多输入多输出非线性系统:

$$\begin{cases} \dot{x}_1 = F_1(\bar{x}_2) + G_1(\bar{x}_2)x_2, \\ \dot{x}_2 = F_2(\bar{x}_2) + G_2(\bar{x}_2)u, \\ y = x_1. \end{cases} \quad (37)$$

其中: $x_1 = [x_{11}, x_{12}]^T$, $x_2 = [x_{21}, x_{22}]^T$, $\bar{x}_2 = [x_1^T, x_2^T]^T$ 是系统的状态; $u = [u_1, u_2]^T$ 是系统的输入; $y = x_1$ 是系统的输出;



(a) 输出 x_{11} 和参考信号 $1/2\sin t$



(b) 输出 x_{12} 和参考信号 $1/2\cos t$

图 1 输出 x 及参考信号

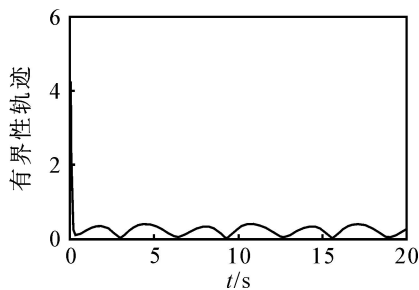
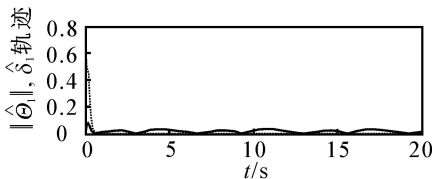
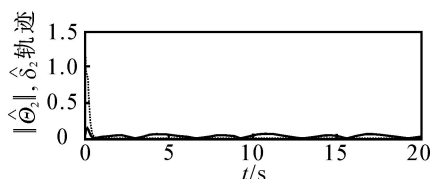


图 2 z_2 的有界性轨迹



(a) $\|\hat{\theta}_1\|$ 和 $\hat{\delta}_1$ 的有界性轨迹



(b) $\|\hat{\theta}_2\|$ 和 $\hat{\delta}_2$ 的有界性轨迹

图 3 $\hat{\theta}$ 和 $\hat{\delta}$ 的有界性轨迹

$F_1(\bar{x}_2) = [f_{11}, f_{12}]^T = [\sin(x_{11}), x_{21}^2]^T$,
 $F_2(\bar{x}_2) = [f_{21}, f_{22}]^T = [3x_{11}e^{-x_{12}}, x_{21} + x_{22}]^T$
 表示系统(37)的不确定部分. 为了方便, 令 $G_1(\bar{x}_2) = G_2(\bar{x}_2) = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$, 初始状态 $x_1(0) = [0 \ 1]^T$, $x_2(0) = [1, -1]^T$, 系统期望的参考输出信号 $y_d(t) = [1/2\sin(t), 1/2\cos(t)]^T$.

利用模糊系统, 未知函数 $F_1(\bar{x}_2)$ 和 $F_2(\bar{x}_2)$ 的逼近值可以分别表示为 $B_1(\bar{x}_2) \wedge_1$ 和 $B_2(x) \wedge_2$. 选择如下隶属度函数:

$$\begin{aligned} \mu_{F_{j,k}^1}(x_{jk}) &= \exp[-0.05(x_{jk} + 10)^2], \\ \mu_{F_{j,k}^2}(x_{jk}) &= \exp[-0.05(x_{jk})^2], \\ \mu_{F_{j,k}^3}(x_{jk}) &= \exp[-0.05(x_{jk} - 10)^2], \\ j &= 1, 2, k = 1, 2, \end{aligned}$$

可以分别得到 $B_1(\bar{x}_2), B_2(\bar{x}_2)$. 选择虚拟控制输入(4)和实际控制输入(30), 自适应律分别选择为(8), (9), (19)和(20), 自适应律的初始值为 $\hat{\wedge}_1(0) = \hat{\wedge}_2(0) = [0, 0, 0]^T$, $\hat{\wedge}_1(0) = \hat{\wedge}_2(0) = 0.5$, 设计参数 $k_1 = k_2 = 3$, $\gamma_1 = \gamma_2 = 0.5$, $\gamma_1 = \gamma_2 = 10$, $\mu_1 = \mu_2 = 10$, $\mu_1^1 = \mu_1^2 = 5$, $\mu_1^3 = \mu_2^3 = 100$, $\mu_1 = \mu_2 = \text{diag}\{2, 2, 2\}$.

通过 Matlab 仿真工具, 可以得到图 1 ~ 图 3. 图 1 为输出和参考信号, 实线为输出, 虚线为参考信号. 可以看出系统的输出很好地跟踪参考输出 $y_d(t)$. 图 2 是误差向量 z_2 的范数有界轨迹. 图 3 的有界性轨迹说明自适应调节参数 $\hat{\wedge}_1, \hat{\wedge}_1, \hat{\wedge}_2, \hat{\wedge}_2$ 是有界的, 实线为 $\hat{\wedge}$, 虚线为 $\hat{\wedge}$ 有界性轨迹.

5 结 语

本文针对不确定非线性 MIMO 纯反馈系统提出一种自适应鲁棒模糊控制方法. 该方法对系统模型进一步放宽了限制条件. 利用 Backstepping 方法的优点和李雅普诺夫稳定性理论, 获得了控制输入和自适应律. 通过选择适当的设计参数, 提出的自适应控制方法使得系统的所有信号是有界的, 并且跟踪误差向量的范数收敛到小的零邻域内.

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$$\bar{R}_{21} = \begin{bmatrix} 0.9415 & -0.021 & 0.546 \\ -0.021 & 3.9063 & 2.0204 \\ 0.546 & 2.0204 & 1.9157 \end{bmatrix},$$

$$\bar{R}_{22} = \begin{bmatrix} 1.0597 & -0.5899 & 0.9238 \\ -0.5899 & 5.6217 & 1.0226 \\ 0.9238 & 1.0226 & 1.8273 \end{bmatrix}.$$

分别给出关联电力系统的输出轨线如图 1, 图 2 所示.

可见 H 控制的镇定效果在约前 4 s 就已经达到, 所以这里提出的控制方法是有效的.

5 结 语

本文研究了一类具有时滞的关联电力系统分散 H 控制问题. 应用 Lyapunov-Krasovskii 泛函方法, 结合时滞积分矩阵不等式技巧, 导出使闭环系统渐近稳定, 且满足一定的 H 性能指标与时滞相关的 LMIs 充分条件, 并给出了分散状态反馈控制器的构造方法. 关联电力系统的仿真示例说明了该方法的有效性.

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