

## 具有区间时变时滞 2-D 离散系统的时滞相关稳定与控制

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**摘要:** 针对具有区间时变时滞 2-D 离散系统, 利用时滞相关方法, 研究其稳定性与控制问题. 首先选取含有时滞项上、下界的一个新的 Lyapunov 函数, 对其差分考虑所有项, 得到了基于线性矩阵不等式 (LMI) 的时滞相关稳定性准则; 然后给定时变时滞项的下界, 再由一个凸优化问题最大化其上界, 进而通过状态反馈实现系统的时滞相关控制, 且求解 LMI 可得到增益矩阵; 最后, 利用数值算例说明了所得结果有效且优于已有成果.

**关键词:** 2-D 离散系统; 区间时变时滞; 时滞相关; 状态反馈; 线性矩阵不等式

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## Delay-dependent stability and control of 2-D discrete systems with interval time-varying delays

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**Abstract:** For 2-D discrete systems with interval time-varying delays, by applying delay-dependent method, the stability and control problems are studied. Firstly, a new Lyapunov functional containing the upper and lower bounds of delays is chosen. Considering all terms in the difference, a new delay-dependent stability criteria based on linear matrix inequalities (LMIs) is derived. Then the lower bounds of time-varying delays are given, and the upper bounds can be maximized through a convex optimization problem. Furthermore, the delay-dependent control is realized through state feedback and the gain matrix can be obtained through solving LMIs. Finally, numerical examples show that the obtained results are effective and better than the existing achievements.

**Key words:** 2-D discrete systems; interval time-varying delays; delay-dependent; state feedback; linear matrix inequality

### 0 引言

由于二维 (2-D) 系统在气体吸收、水流加热和空气干燥等现代工程领域广泛存在<sup>[1]</sup>, 过去的几十年里, 已引起了许多学者的研究兴趣<sup>[2-4]</sup>. 在一些 2-D 系统中时滞是不可避免的, 而时滞的存在通常是造成系统不稳定和破坏系统性能的根源, 因此, 对 2-D 时滞系统的研究是非常必要的. 文献 [5-7] 分别考虑了 2-D 时滞系统的稳定性、控制和滤波问题, 但只限于时滞无关方法. 基于时滞相关方法, 文献 [8-10] 给出了 2-D 时滞系统时滞相关稳定性准则和状态反馈控制器设计

方法. 文献 [11-12] 进一步考虑了输出反馈  $H_\infty$  控制与滤波问题.

鉴于时变时滞情形在实际系统中更为常见, 为了降低保守性, 文献 [13] 利用改进的权值调整方法, 考虑了不确定 2-D 时滞系统的时滞相关稳定性分析和控制综合问题, 其结果由线性矩阵不等式 (LMI) 给出. 对于具有区间时变时滞的 2-D 马尔可夫跳跃系统, 文献 [14] 将 Jensen 不等式引入 Lyapunov 函数差分中, 研究了系统的时滞相关滤波问题. 虽然 Jensen 不等式的引入大大减少了待定矩阵的数量, 减轻了运算负担,

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但会增加差分上界, 导致结果保守性增强. 为此, 文献 [15] 针对非线性 2-D 时变时滞系统, 通过引入含时滞上下界的 Lyapunov 函数, 研究了系统的稳定和控制问题, 但仍限于时滞无关方法.

针对上述研究成果的局限性, 本文进一步研究具有区间时变时滞 2-D 离散系统的稳定和控制问题. 通过引入含有时变时滞项上下界的 Lyapunov 函数, 在差分时考虑到和式所有项并结合权值调整方法<sup>[13]</sup>, 提出了系统的时滞相关稳定性准则. 进而, 设计状态反馈增益矩阵, 实现了系统的稳定控制. 稳定性和控制结果均由 LMI 给出, 通过求解一个凸优化问题, 可以得到时滞项上界的最大值. 最后, 通过数值算例验证了本文研究结果的有效性.

## 1 问题描述

考虑 2-D 区间时变时滞系统

$$\begin{aligned} x(i+1, j+1) = & \\ & A_1x(i+1, j) + A_2x(i, j+1) + \\ & A_{1d}x(i+1, j-d_1(j)) + A_{2d}x(i-d_2(i), j+1) + \\ & B_1u(i+1, j) + B_2u(i, j+1). \end{aligned} \quad (1)$$

其中:  $x(i, j) \in R^n$  是状态向量;  $u(i, j) \in R^m$  是系统的控制输入;  $A_k, A_{kd}, B_k$  ( $k = 1, 2$ ) 是具有相应维数的常数矩阵;  $d_1(j)$  和  $d_2(i)$  是时变时滞项, 且满足

$$\begin{aligned} 0 < d_{1m} \leq d_1(j) \leq d_{1M}, \\ 0 < d_{2m} \leq d_2(i) \leq d_{2M}. \end{aligned} \quad (2)$$

系统 (1) 的边界条件具有如下形式:

$$\begin{aligned} \{x(i, j) = \varphi_{i,j}\}, \forall i \geq 0, \\ j = -d_{1M}, -d_{1M} + 1, \dots, 0; \\ \{x(i, j) = \psi_{i,j}\}, \forall j \geq 0, \\ i = -d_{2M}, -d_{2M} + 1, \dots, 0; \\ \varphi_{0,0} = \psi_{0,0}. \end{aligned} \quad (3)$$

其中函数  $\varphi_{i,j}$  和  $\psi_{i,j}$  满足

$$\sum_{i=0}^{\infty} \sum_{j=-d_1}^0 \varphi_{i,j}^T \varphi_{i,j} < \infty, \quad \sum_{j=0}^{\infty} \sum_{i=-d_2}^0 \psi_{i,j}^T \psi_{i,j} < \infty.$$

选取 2-D 状态反馈控制器

$$u(i, j) = Kx(i, j), \quad (4)$$

其中  $K$  是状态反馈增益矩阵, 则闭环系统可表示为

$$\begin{aligned} x(i+1, j+1) = & \\ & (A_1 + B_1K)x(i+1, j) + (A_2 + B_2K)x(i, j+1) + \\ & A_{1d}x(i+1, j-d_1(j)) + A_{2d}x(i-d_2(i), j+1). \end{aligned} \quad (5)$$

本文将得到具有区间时变时滞 2-D 离散系统 (1) ( $u(i, j) = 0$ ) 的时滞相关稳定性准则, 并通过状态反馈控制器 (4) 实现系统 (1) 的稳定控制.

## 2 时滞相关稳定性准则

首先分析 2-D 区间时变时滞系统 (1) ( $u(i, j) = 0$ ) 的稳定性. 下面的定理给出了系统的时滞相关稳定性准则.

**定理 1** 给定  $d_{km}$  和  $d_{kM}$  ( $0 < d_{km} < d_{kM}, k = 1, 2$ ), 对于具有边界条件 (3), 且时滞项  $d_1(j)$  和  $d_2(i)$  满足式 (2) 的 2-D 系统 (1) ( $u(i, j) = 0$ ), 如果存在  $P > 0, Q > 0, R_{kl} \geq 0, Q_k \geq 0, S_k > 0, Z_k > 0$ , 以及

$$\begin{aligned} X_k = \begin{bmatrix} X_{k1} & X_{k2} \\ * & X_{k3} \end{bmatrix} \geq 0, \quad Y_k = \begin{bmatrix} Y_{k1} & Y_{k2} \\ * & Y_{k3} \end{bmatrix} \geq 0, \\ N_k = \begin{bmatrix} N_{k1} \\ N_{k2} \end{bmatrix}, \quad M_k = \begin{bmatrix} M_{k1} \\ M_{k2} \end{bmatrix}, \quad T_k = \begin{bmatrix} T_{k1} \\ T_{k2} \end{bmatrix}, \\ k, l = 1, 2, \end{aligned}$$

使得如下 LMI 成立:

$$\begin{bmatrix} \Psi_1 & \Psi_2 & \Psi_3 \\ * & \Psi_4 & 0 \\ * & * & \Psi_5 \end{bmatrix} < 0, \quad (6)$$

$$\Xi_{k1} = \begin{bmatrix} X_{k1} & X_{k2} & N_{k1} \\ * & X_{k3} & N_{k2} \\ * & * & S_k \end{bmatrix} \geq 0, \quad (7)$$

$$\Xi_{k2} = \begin{bmatrix} X_{k1} + Y_{k1} & X_{k2} + Y_{k2} & M_{k1} \\ * & X_{k3} + Y_{k3} & M_{k2} \\ * & * & S_k + Z_k \end{bmatrix} \geq 0, \quad (8)$$

$$\Xi_{k3} = \begin{bmatrix} Y_{k1} & Y_{k2} & T_{k1} \\ * & Y_{k3} & T_{k2} \\ * & * & Z_k \end{bmatrix} \geq 0, \quad k = 1, 2, \quad (9)$$

则系统是渐近稳定的. 式 (6) 中

$$\Psi_1 = \begin{bmatrix} \Psi_{11} & 0 & \Psi_{13} & 0 \\ * & \Psi_{22} & 0 & \Psi_{24} \\ * & * & \Psi_{33} & 0 \\ * & * & * & \Psi_{44} \end{bmatrix},$$

$$\Psi_{11} = R_{11} + R_{21} + (d_{12} + 1)Q_1 - Q +$$

$$N_{11} + N_{11}^T + d_{1M}X_{11} + d_{12}Y_{11},$$

$$\Psi_{22} = R_{12} + R_{22} + (d_{21} + 1)Q_2 - P + Q +$$

$$N_{21} + N_{21}^T + d_{2M}X_{21} + d_{21}Y_{21},$$

$$d_{12} = d_{1M} - d_{1m}, \quad d_{21} = d_{2M} - d_{2m},$$

$$\Psi_{13} = N_{12}^T - N_{11} + M_{11} - T_{11} + d_{1M}X_{12} + d_{12}Y_{12},$$

$$\Psi_{24} = N_{22}^T - N_{21} + M_{21} - T_{21} + d_{2M}X_{22} + d_{21}Y_{22},$$

$$\Psi_{33} = -Q_1 - N_{12}^T - N_{12} + M_{12} + M_{12}^T -$$

$$T_{12} - T_{12}^T + d_{1M}X_{13} + d_{12}Y_{13},$$

$$\Psi_{44} = -Q_2 - N_{22}^T - N_{22} + M_{22} + M_{22}^T -$$

$$T_{22} - T_{22}^T + d_{2M}X_{23} + d_{21}Y_{23},$$

$$\Psi_2 = \begin{bmatrix} T_{11} & 0 & -M_{11} & 0 \\ 0 & T_{21} & 0 & -M_{21} \\ T_{12} & 0 & -M_{12} & 0 \\ 0 & T_{22} & 0 & -M_{22} \end{bmatrix},$$

$$\Psi_3 = [\Phi_1^T P \quad d_{1M} \Phi_{21}^T S_1 \quad d_{12} \Phi_{21}^T Z_1 \rightarrow \\ \leftarrow d_{2M} \Phi_{22}^T S_2 \quad d_{21} \Phi_{22}^T Z_2],$$

$$\Phi_1 = [A_1 \quad A_2 \quad A_{1d} \quad A_{2d}],$$

$$\Phi_{21} = [A_1 - I \quad A_2 \quad A_{1d} \quad A_{2d}],$$

$$\Phi_{22} = [A_1 \quad A_2 - I \quad A_{1d} \quad A_{2d}],$$

$$\Psi_4 = \text{diag}\{-R_{21}, -R_{22}, -R_{11}, -R_{12}\},$$

$$\Psi_5 = \text{diag}\{-P, -d_{1M}S_1, -d_{12}Z_1, \\ -d_{2M}S_2, -d_{21}Z_2\}.$$

证明 记  $x_{\xi,\eta} = x(i + \xi, j + \eta)$  和

$$\bar{y}_{1,l} = x_{1,l+1} - x_{1,l}, \quad \bar{y}_{l,1} = x_{l+1,1} - x_{l,1}. \quad (10)$$

选取 Lyapunov 函数

$$V_{11} =$$

$$x_{1,1}^T P x_{1,1} + \sum_{l=-d_{1M}}^{-1} x_{1,l+1}^T R_{11} x_{1,l+1} + \\ \sum_{l=-d_{2M}}^{-1} x_{l+1,1}^T R_{12} x_{l+1,1} + \sum_{l=-d_{1m}}^{-1} x_{1,l+1}^T R_{21} x_{1,l+1} + \\ \sum_{l=-d_{2m}}^{-1} x_{l+1,1}^T R_{22} x_{l+1,1} + \\ \sum_{\theta=-d_{1M}}^{-d_{1m}} \sum_{l=\theta}^{-1} x_{1,l+1}^T Q_1 x_{1,l+1} + \\ \sum_{\theta=-d_{2M}}^{-d_{2m}} \sum_{l=\theta}^{-1} x_{l+1,1}^T Q_2 x_{l+1,1} + \\ \sum_{\theta=-d_{1M}}^{-1} \sum_{l=\theta}^{-1} \bar{y}_{1,l+1}^T S_1 \bar{y}_{1,l+1} + \\ \sum_{\theta=-d_{1M}}^{-d_{1m}-1} \sum_{l=\theta}^{-1} \bar{y}_{1,l+1}^T Z_1 \bar{y}_{1,l+1} + \\ \sum_{\theta=-d_{2M}}^{-1} \sum_{l=\theta}^{-1} \bar{y}_{l+1,1}^T S_2 \bar{y}_{l+1,1} + \\ \sum_{\theta=-d_{2M}}^{-d_{2m}-1} \sum_{l=\theta}^{-1} \bar{y}_{l+1,1}^T Z_2 \bar{y}_{l+1,1},$$

$$V_{d1} =$$

$$x_{1,0}^T Q x_{1,0} + \sum_{l=-d_{1M}}^{-1} x_{1,l}^T R_{11} x_{1,l} + \\ \sum_{l=-d_{1m}}^{-1} x_{1,l}^T R_{21} x_{1,l} + \sum_{\theta=-d_{1M}}^{-d_{1m}} \sum_{l=\theta}^{-1} x_{1,l}^T Q_1 x_{1,l} +$$

$$\sum_{\theta=-d_{1M}}^{-1} \sum_{l=\theta}^{-1} \bar{y}_{1,l}^T S_1 \bar{y}_{1,l} + \sum_{\theta=-d_{1M}}^{-d_{1m}-1} \sum_{l=\theta}^{-1} \bar{y}_{1,l}^T Z_1 \bar{y}_{1,l},$$

$$V_{d2} =$$

$$x_{0,1}^T (P - Q) x_{0,1} + \sum_{l=-d_{2M}}^{-1} x_{l,1}^T R_{12} x_{l,1} + \\ \sum_{l=-d_{2m}}^{-1} x_{l,1}^T R_{22} x_{l,1} + \sum_{\theta=-d_{2M}}^{-d_{2m}} \sum_{l=\theta}^{-1} x_{l,1}^T Q_2 x_{l,1} + \\ \sum_{\theta=-d_{2M}}^{-1} \sum_{l=\theta}^{-1} \bar{y}_{l,1}^T S_2 \bar{y}_{l,1} + \sum_{\theta=-d_{2M}}^{-d_{2m}-1} \sum_{l=\theta}^{-1} \bar{y}_{l,1}^T Z_2 \bar{y}_{l,1}. \quad (11)$$

其中:  $P > 0, Q > 0, R_{kl} \geq 0, Q_k \geq 0, S_k > 0$  且  $Z_k > 0 (k, l = 1, 2)$  为待定.

根据式 (10), 对于具有相应维数的任意矩阵  $N_k, M_k$  和  $T_k (k = 1, 2)$ , 有

$$0 = 2\xi_2^{(1)T} N_1 \left[ x_{1,0} - x_{1,-d_1(j)} - \sum_{l=-d_1(j)}^{-1} \bar{y}_{1,l} \right], \\ 0 = 2\xi_2^{(2)T} N_2 \left[ x_{0,1} - x_{-d_2(i),1} - \sum_{l=-d_2(i)}^{-1} \bar{y}_{l,1} \right], \\ 0 = 2\xi_2^{(1)T} M_1 \left[ x_{1,-d_1(j)} - x_{1,-d_{1M}} - \sum_{l=-d_{1M}}^{-d_1(j)-1} \bar{y}_{1,l} \right], \\ 0 = 2\xi_2^{(2)T} M_2 \left[ x_{-d_2(i),1} - x_{-d_{2M},1} - \sum_{l=-d_{2M}}^{-d_2(i)-1} \bar{y}_{l,1} \right], \\ 0 = 2\xi_2^{(1)T} T_1 \left[ x_{1,-d_{1m}} - x_{1,-d_1(j)} - \sum_{l=-d_1(j)}^{-d_{1m}-1} \bar{y}_{1,l} \right], \\ 0 = 2\xi_2^{(2)T} T_2 \left[ x_{-d_{2m},1} - x_{-d_2(i),1} - \sum_{l=-d_2(i)}^{-d_{2m}-1} \bar{y}_{l,1} \right], \\ \xi_2^{(1)} = [x_{1,0}^T \quad x_{1,-d_1(j)}^T]^T, \quad \xi_2^{(2)} = [x_{0,1}^T \quad x_{-d_2(i),1}^T]^T. \quad (12)$$

另一方面, 对于具有相应维数的矩阵  $X_k \geq 0$  和  $Y_k \geq 0 (k = 1, 2)$ , 下面等式成立:

$$0 = \sum_{l=-d_{1M}}^{-1} \xi_2^{(1)T} X_1 \xi_2^{(1)} - \sum_{l=-d_{1M}}^{-1} \xi_2^{(1)T} X_1 \xi_2^{(1)} = \\ d_{1M} \xi_2^{(1)T} X_1 \xi_2^{(1)} - \sum_{l=-d_1(j)}^{-1} \xi_2^{(1)T} X_1 \xi_2^{(1)} - \\ \sum_{l=-d_{1M}}^{-d_1(j)-1} \xi_2^{(1)T} X_1 \xi_2^{(1)}, \\ 0 = \sum_{l=-d_{2M}}^{-1} \xi_2^{(2)T} X_2 \xi_2^{(2)} - \sum_{l=-d_{2M}}^{-1} \xi_2^{(2)T} X_2 \xi_2^{(2)} = \\ d_{2M} \xi_2^{(2)T} X_2 \xi_2^{(2)} - \sum_{l=-d_2(i)}^{-1} \xi_2^{(2)T} X_2 \xi_2^{(2)} -$$

$$\begin{aligned}
& \sum_{l=-d_{2M}}^{-d_2(i)-1} \xi_2^{(2)T} X_2 \xi_2^{(2)}, \\
0 = & \sum_{l=-d_{1M}}^{-d_{1m}-1} \xi_2^{(1)T} Y_1 \xi_2^{(1)} - \sum_{l=-d_{1M}}^{-d_{1m}-1} \xi_2^{(1)T} Y_1 \xi_2^{(1)} = \\
& d_{12} \xi_2^{(1)T} Y_1 \xi_2^{(1)} - \sum_{l=-d_1(j)}^{-d_{1m}-1} \xi_2^{(1)T} Y_1 \xi_2^{(1)} - \\
& \sum_{l=-d_{1M}}^{-d_1(j)-1} \xi_2^{(1)T} Y_1 \xi_2^{(1)}, \\
0 = & \sum_{l=-d_{2M}}^{-d_{2m}-1} \xi_2^{(2)T} Y_2 \xi_2^{(2)} - \sum_{l=-d_{2M}}^{-d_{2m}-1} \xi_2^{(2)T} Y_2 \xi_2^{(2)} = \\
& d_{21} \xi_2^{(2)T} Y_2 \xi_2^{(2)} - \sum_{l=-d_2(i)}^{-d_{2m}-1} \xi_2^{(2)T} Y_2 \xi_2^{(2)} - \\
& \sum_{l=-d_{2M}}^{-d_2(i)-1} \xi_2^{(2)T} Y_2 \xi_2^{(2)}. \quad (13)
\end{aligned}$$

现在, 定义 Lyapunov 函数 (11) 的差分为  $\Delta V = V_{11} - V_{d1} - V_{d2}$ , 加上等式 (12) 和 (13) 的右端, 有

$$\begin{aligned}
\Delta V \leq & \xi_1^T [\Phi_1^T P \Phi_1 + \Phi_2^{(1)T} (d_{1M} S_1 + d_{12} Z_1) \Phi_2^{(1)} + \\
& \Phi_2^{(2)T} (d_{2M} S_2 + d_{21} Z_2) \Phi_2^{(2)} + \Psi] \xi_1 - \\
& \sum_{l=-d_1(j)}^{-1} \xi_3^{(1)T} \Xi_{11} \xi_3^{(1)} - \sum_{l=-d_2(i)}^{-1} \xi_3^{(2)T} \Xi_{21} \xi_3^{(2)} - \\
& \sum_{l=-d_{1M}}^{-d_1(j)-1} \xi_3^{(1)T} \Xi_{12} \xi_3^{(1)} - \sum_{l=-d_{2M}}^{-d_2(i)-1} \xi_3^{(2)T} \Xi_{22} \xi_3^{(2)} - \\
& \sum_{l=-d_{1M}}^{-d_{1m}-1} \xi_3^{(1)T} \Xi_{13} \xi_3^{(1)} - \sum_{l=-d_{2M}}^{-d_{2m}-1} \xi_3^{(2)T} \Xi_{23} \xi_3^{(2)}. \quad (14)
\end{aligned}$$

其中

$$\begin{aligned}
\xi_1 = & [x_{1,0}^T, x_{0,1}^T, x_{1,-d_1(j)}^T, x_{-d_2(i),1}^T, x_{1,-d_{1m}}^T, \\
& x_{-d_{2m},1}^T, x_{1,-d_{1M}}^T, x_{-d_{2M},1}^T]^T, \\
\xi_3^{(1)} = & [\xi_2^{(1)T} \bar{y}_{1,l}^T, \xi_3^{(2)} = [\xi_2^{(2)T} \bar{y}_{l,1}^T]^T.
\end{aligned}$$

如果  $\Xi_{kl} \geq 0$  ( $k = 1, 2; l = 1, 2, 3$ ) 和  $\Phi_1^T P \Phi_1 + \Phi_2^{(1)T} (d_{1M} S_1 + d_{12} Z_1) \Phi_2^{(1)} + \Phi_2^{(2)T} (d_{2M} S_2 + d_{21} Z_2) \Phi_2^{(2)} + \Psi < 0$  成立, 即由 Schur 补性质等价于式 (7) ~ (9) 和 (6), 则  $\Delta V < 0$ , 即系统 (1) ( $u(i, j) = 0$ ) 渐近稳定.  $\square$

**注 1** 在定理 1 的证明中, 当计算 Lyapunov 函数差分,  $d_{1M}$  和  $d_{2M}$  都被分成两部分:  $d_{1M} = d_1(j) + (d_{1M} - d_1(j))$  和  $d_{2M} = d_2(i) + (d_{2M} - d_2(i))$ . 因此, 在 Lyapunov 函数差分过程中, 求和项没有任何增加, 从而降低了结果的保守性.

**注 2** 给定时滞项  $d_1(j)$  和  $d_2(i)$  的下界及  $d_1(j)$  的上界, 利用 Matlab 的 GEVP 求解器求解如下凸优化

问题:

$$\begin{aligned}
& \text{最小化 } \delta \text{ 使得 } P > 0, Q > 0, R_{kl} \geq 0, \\
& Q_k \geq 0, S_k > 0, Z_k > 0, X_k \geq 0, Y_k \geq 0, \\
& k, l = 1, 2, \text{ 和式 (6) ~ (9) 成立,}
\end{aligned}$$

可以得到  $d_2(i)$  的最大化上界, 其中  $\delta = 1/d_{2M}$ . 类似地, 也可以求得  $d_1(j)$  的最大化上界.

### 3 时滞相关状态反馈控制器设计

下面针对 2-D 区间时变时滞系统 (1) 设计状态反馈控制器 (4), 使得闭环系统 (5) 渐近稳定. 直接应用定理 1 于闭环系统 (5) 可得如下定理.

**定理 2** 给定常数  $t, t_k, t_{k+2}, d_{km}$  和  $d_{kM}$  ( $0 < d_{km} < d_{kM}, k = 1, 2$ ), 对于边界条件满足式 (3) 且时滞项  $d_1(j), d_2(i)$  满足式 (2) 的 2-D 系统 (1), 设计状态反馈控制器 (4), 如果存在矩阵  $\tilde{U} > 0, \tilde{Q} > 0, \tilde{R}_{kl} \geq 0, \tilde{Q}_k \geq 0$ , 以及

$$\begin{aligned}
\tilde{X}_k = & \begin{bmatrix} \tilde{X}_{k1} & \tilde{X}_{k2} \\ * & \tilde{X}_{k3} \end{bmatrix} \geq 0, \tilde{Y}_k = \begin{bmatrix} \tilde{Y}_{k1} & \tilde{Y}_{k2} \\ * & \tilde{Y}_{k3} \end{bmatrix} \geq 0, \\
\tilde{N}_k = & \begin{bmatrix} \tilde{N}_{k1} \\ \tilde{N}_{k2} \end{bmatrix}, \tilde{M}_k = \begin{bmatrix} \tilde{M}_{k1} \\ \tilde{M}_{k2} \end{bmatrix}, \tilde{T}_k = \begin{bmatrix} \tilde{T}_{k1} \\ \tilde{T}_{k2} \end{bmatrix}, \\
& k, l = 1, 2
\end{aligned}$$

和  $V$ , 使得如下 LMI 成立:

$$\begin{bmatrix} \tilde{\Psi}_1 & \tilde{\Psi}_2 & \tilde{\Psi}_3 \\ * & \tilde{\Psi}_4 & 0 \\ * & * & \tilde{\Psi}_5 \end{bmatrix} < 0, \quad (15)$$

$$\tilde{\Xi}_{k1} = \begin{bmatrix} \tilde{X}_{k1} & \tilde{X}_{k2} & \tilde{N}_{k1} \\ * & \tilde{X}_{k3} & \tilde{N}_{k2} \\ * & * & t_k \tilde{U} \end{bmatrix} \geq 0, \quad (16)$$

$$\tilde{\Xi}_{k2} = \begin{bmatrix} \tilde{X}_{k1} + \tilde{Y}_{k1} & \tilde{X}_{k2} + \tilde{Y}_{k2} & \tilde{M}_{k1} \\ * & \tilde{X}_{k3} + \tilde{Y}_{k3} & \tilde{M}_{k2} \\ * & * & (t_k + t_{k+2}) \tilde{U} \end{bmatrix} \geq 0, \quad (17)$$

$$\tilde{\Xi}_{k3} = \begin{bmatrix} \tilde{Y}_{k1} & \tilde{Y}_{k2} & \tilde{T}_{k1} \\ * & \tilde{Y}_{k3} & \tilde{T}_{k2} \\ * & * & t_{k+2} \tilde{U} \end{bmatrix} \geq 0, \quad k = 1, 2, \quad (18)$$

则闭环系统 (5) 渐近稳定. 式 (15) 中

$$\tilde{\Psi}_1 = \begin{bmatrix} \tilde{\Psi}_{11} & 0 & \tilde{\Psi}_{13} & 0 \\ * & \tilde{\Psi}_{22} & 0 & \tilde{\Psi}_{24} \\ * & * & \tilde{\Psi}_{33} & 0 \\ * & * & * & \tilde{\Psi}_{44} \end{bmatrix},$$

$$\tilde{\Psi}_{11} = \tilde{R}_{11} + \tilde{R}_{21} + (d_{12} + 1) \tilde{Q}_1 - \tilde{Q} +$$

$$\tilde{N}_{11} + \tilde{N}_{11}^T + d_{1M} \tilde{X}_{11} + d_{12} \tilde{Y}_{11},$$

$$\tilde{\Psi}_{22} = \tilde{R}_{12} + \tilde{R}_{22} + (d_{21} + 1) \tilde{Q}_2 - t \tilde{U} + \tilde{Q} +$$

$$\begin{aligned}
 & \tilde{N}_{21} + \tilde{N}_{21}^T + d_{2M}\tilde{X}_{21} + d_{21}\tilde{Y}_{21}, \\
 \tilde{\Psi}_{13} = & \tilde{N}_{12}^T - \tilde{N}_{11} + \tilde{M}_{11} - \tilde{T}_{11} + \\
 & d_{1M}\tilde{X}_{12} + d_{12}\tilde{Y}_{12}, \\
 \tilde{\Psi}_{24} = & \tilde{N}_{22}^T - \tilde{N}_{21} + \tilde{M}_{21} - \tilde{T}_{21} + \\
 & d_{2M}\tilde{X}_{22} + d_{21}\tilde{Y}_{22}, \\
 \tilde{\Psi}_{33} = & -\tilde{Q}_1 - \tilde{N}_{12}^T - \tilde{N}_{12} + \tilde{M}_{12} + \tilde{M}_{12}^T - \\
 & \tilde{T}_{12} - \tilde{T}_{12}^T + d_{1M}\tilde{X}_{13} + d_{12}\tilde{Y}_{13}, \\
 \tilde{\Psi}_{44} = & -\tilde{Q}_2 - \tilde{N}_{22}^T - \tilde{N}_{22} + \tilde{M}_{22} + \tilde{M}_{22}^T - \\
 & \tilde{T}_{22} - \tilde{T}_{22}^T + d_{2M}\tilde{X}_{23} + d_{21}\tilde{Y}_{23}, \\
 \tilde{\Psi}_2 = & \begin{bmatrix} \tilde{T}_{11} & 0 & -\tilde{M}_{11} & 0 \\ 0 & \tilde{T}_{21} & 0 & -\tilde{M}_{21} \\ \tilde{T}_{12} & 0 & -\tilde{M}_{12} & 0 \\ 0 & \tilde{T}_{22} & 0 & -\tilde{M}_{22} \end{bmatrix}, \\
 \tilde{\Psi}_3 = & [t\tilde{\Phi}_1^T \quad t_1d_{1M}\tilde{\Phi}_{21}^T \quad t_3d_{12}\tilde{\Phi}_{21}^T \rightarrow \\
 & \leftarrow t_2d_{2M}\tilde{\Phi}_{22}^T \quad t_4d_{21}\tilde{\Phi}_{22}^T], \\
 \tilde{\Phi}_1 = & [\tilde{A}_1 \quad \tilde{A}_2 \quad A_{1d}\tilde{U} \quad A_{2d}\tilde{U}], \\
 \tilde{\Phi}_{21} = & [\tilde{A}_1 - \tilde{U} \quad \tilde{A}_2 \quad A_{1d}\tilde{U} \quad A_{2d}\tilde{U}], \\
 \tilde{\Phi}_{22} = & [\tilde{A}_1 \quad \tilde{A}_2 - \tilde{U} \quad A_{1d}\tilde{U} \quad A_{2d}\tilde{U}], \\
 \tilde{A}_k^T = & \tilde{U}A_k^T + V^TB_k^T, \quad k = 1, 2, \\
 \tilde{\Psi}_4 = & \text{diag}\{-\tilde{R}_{21}, -\tilde{R}_{22}, -\tilde{R}_{11}, -\tilde{R}_{12}\}, \\
 \tilde{\Psi}_5 = & \text{diag}\{-t\tilde{U}, -t_1d_{1M}\tilde{U}, -t_3d_{12}\tilde{U}, \\
 & -t_2d_{2M}\tilde{U}, -t_4d_{21}\tilde{U}\}, \\
 V = & K\tilde{U}. \tag{19}
 \end{aligned}$$

**证明** 将定理1应用于闭环系统(5), 在式(6)中用  $A_k + B_kK$  代替  $A_k$  ( $k = 1, 2$ ), 再令

$$\begin{aligned}
 P &= tU, \quad S_k = t_kU, \quad Z_k = t_{k+2}U, \\
 V &= K\tilde{U} (\tilde{U} = U^{-1}), \quad \tilde{Q} = \tilde{U}Q\tilde{U}, \quad \tilde{R}_{kl} = \tilde{U}R_{kl}\tilde{U}, \\
 \tilde{N}_{kl} &= \tilde{U}N_{kl}\tilde{U}, \quad \tilde{M}_{kl} = \tilde{U}M_{kl}\tilde{U}, \quad \tilde{T}_{kl} = \tilde{U}T_{kl}\tilde{U}, \\
 \tilde{Q}_k &= \tilde{U}Q_k\tilde{U}, \quad \tilde{X}_{kL} = \tilde{U}X_{kL}\tilde{U}, \\
 \tilde{Y}_{kL} &= \tilde{U}Y_{kL}\tilde{U}, \quad k, l = 1, 2, \quad L = 1, 2, 3.
 \end{aligned}$$

用  $\text{diag}\{\tilde{U}, \tilde{U}, \tilde{U}\}$  左乘和右乘式(6), 则式(15)成立. 类似地, 用  $\text{diag}\{\tilde{U}, \tilde{U}, \tilde{U}\}$  左乘和右乘式(7)~(9), 可得式(16)~(18)成立.  $\square$

**注3** 由于  $P > 0, S_k > 0$  和  $Z_k > 0$  ( $k = 1, 2$ ), 有  $\tilde{U} > 0$ . 进而, 可求得状态反馈控制器为

$$u(i, j) = V\tilde{U}^{-1}x(i, j). \tag{20}$$

### 4 数值算例

**例1** 考虑本文结果在实际系统中的应用. 采用文献[9]中的例子, 由偏微分方程表示具有时滞的热处理过程可用2-DFM模型(1) ( $u(i, j) = 0$ ) 描述, 系

统参数为

$$\begin{aligned}
 A_1 &= \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, \quad A_2 = \begin{bmatrix} 0 & 0 \\ 0.25 & 0.65 \end{bmatrix}, \\
 A_{1d} &= \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, \quad A_{2d} = \begin{bmatrix} 0 & 0 \\ 0 & -0.12 \end{bmatrix}. \tag{21}
 \end{aligned}$$

该系统的稳定性无法由文献[5]中的时滞无关准则求解. 当时滞为定常, 即  $d_1(j) = h_2$  时, 文献[9]说明对于任意常时滞  $h_2$  满足  $0 < h_2 \leq 5$ , 系统渐近稳定; 当时滞  $d_1(j)$  为时变且  $0 \leq d_1(j) \leq 13$  时, 文献[13]证明了系统的稳定性, 即  $d_1(j)$  的上界比文献[9]给出的大很多. 应用本文提出的定理1, 对于  $0 \leq d_1(j) \leq 20$ , 系统仍渐近稳定, 表明本文得到的最大化上界比文献[13]中的还大. 图1给出了时滞  $d_1(j)$  上界为20的系统(21)状态轨迹, 显然系统渐近稳定.

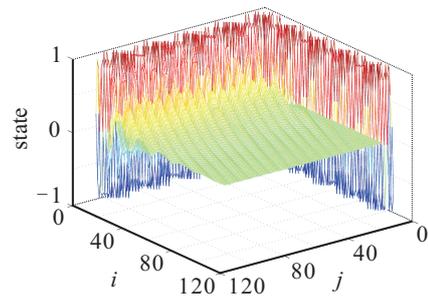


图1 时滞上界  $d_{1M}$  为20的系统(21)的状态轨迹

**例2** 考虑系统(1) ( $u(i, j) = 0$ ) 的渐近稳定性. 系统参数为

$$\begin{aligned}
 A_1 &= \begin{bmatrix} 0 & 0.6 \\ 0 & 0.2 \end{bmatrix}, \quad A_2 = \begin{bmatrix} 0 & 0 \\ 0.2 & 0.65 \end{bmatrix}, \\
 A_{1d} &= \begin{bmatrix} 0 & 0 \\ -0.1 & 0 \end{bmatrix}, \quad A_{2d} = \begin{bmatrix} 0 & 0 \\ 0 & -0.1 \end{bmatrix}. \tag{22}
 \end{aligned}$$

系统的稳定性无法由文献[5]中的时滞无关方法分析. 应用文献[13]的定理1和本文的注2分别可得  $d_{1j}$  的最大化上界, 由表1给出. 很显然, 本文提出的方法更适用于实际中时滞不可避免的情形(即时滞下界大于零), 且  $d_{1j}$  的最大上界可以无限大, 明显优于应用文献[13]定理1所求的  $d_{1j}$  最大上界. 此外, 图2描述了时滞项  $d_{1j}$  上界任意大时系统(22)的状态轨迹, 该系统稳定.

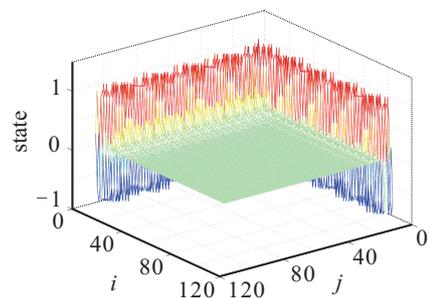


图2 时滞上界  $d_{1M}$  任意大时系统(22)的状态轨迹

表1 给定  $d_{1m}, d_{2m}$  和  $d_{2M}, d_1(j)$  的最大化上界

方法	$d_{1m}$	$d_{1M}(\tau_1)$	$d_{2m}$	$d_{2M}(\tau_2)$
文献[13]	0	4	0	10
本文定理1	1	任意大	1	10

例3 考虑2-D系统(1), 具有以下参数:

$$A_1 = \begin{bmatrix} 0 & 1 \\ 0 & 0.5 \end{bmatrix}, A_2 = \begin{bmatrix} 0 & 0.5 \\ 0 & 0.5 \end{bmatrix},$$

$$A_{1d} = \begin{bmatrix} 0 & 0.25 \\ -0.2 & 0 \end{bmatrix}, A_{2d} = \begin{bmatrix} 0.2 & 0 \\ 0 & 0.3 \end{bmatrix},$$

$$B_1 = \begin{bmatrix} 0.2 & 0 \\ 0.1 & 0 \end{bmatrix}, B_2 = \begin{bmatrix} 0.4 & 0 \\ 0.8 & 0 \end{bmatrix}, \quad (23)$$

且时滞项满足  $1 \leq d_1(j) \leq 20, 3 \leq d_2(i) \leq 11$ .

应用定理2, 给定  $t = 2, t_1 = 3, t_2 = 0.3, t_3 = 1, t_4 = 0.5$ , 状态反馈控制问题可解并由式(20)可得

$$K = V\tilde{U}^{-1} = \begin{bmatrix} 0.1113 & -0.5742 \\ 0 & 0 \end{bmatrix}. \quad (24)$$

图3表明, 上述增益可保证系统(23)的稳定性.

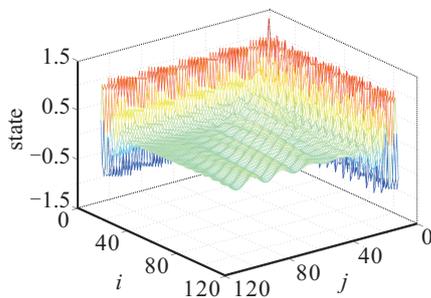


图3 具有状态反馈增益(24)的系统(23)的状态轨迹

## 5 结论

本文研究了具有区间时变时滞2-D系统的稳定和控制问题. 通过选取含有时变时滞项上下界的Lyapunov函数, 差分考虑到和式的所有项, 并引入自由加权矩阵, 得到了保守性较小的时滞相关稳定条件, 同时将时滞项上界最大化. 进而, 设计状态反馈控制器以保证系统的稳定性, 且可由LMI求得控制增益矩阵. 最后, 利用数值算例验证了本文所得结果有效并优于已有成果.

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