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## 基于 Jensen 不等式的 2-D 区间时变时滞系统的稳定与控制

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**摘要:** 考虑具有区间时变时滞二维(2-D)离散系统的时滞相关稳定性和控制问题. 选取含有时滞上下界的 Lyapunov 函数, 对其差分时考虑到所有项, 结合 2-D Jensen 不等式, 由线性矩阵不等式给出系统新的时滞相关稳定性准则. 准则中含有更少的待定变量, 降低了数值计算负担, 并且比一些已有结果具有更小的保守性. 基于稳定性准则, 由状态反馈实现了系统的稳定控制. 最后, 通过数值算例表明了所得结果的有效性和优越性.

**关键词:** 2-D 离散系统; 区间时变时滞; 时滞相关; 2-D Jensen 不等式; 状态反馈

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## Stability and control of 2-D interval time-varying delay systems based on Jensen inequality

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**Abstract:** This paper concerns the problems of delay-dependent stability and control for 2-D discrete systems with interval time-varying delays. By choosing a Lyapunov functional with the upper and lower bounds of delays and considering all terms in its difference, then combining with the 2-D Jensen inequalities, a new delay-dependent stability criteria is given in terms of linear matrix inequalities(LMIs). Less decision variables are involved in the criteria, so the burden of numerical computation is reduced. And it is less conservative than some existing ones. Based on the stability criteria, state feedback is considered to realize the stability control of the system. Finally, numerical examples are given to illustrate the effectiveness and advantage of the results.

**Keywords:** 2-D discrete systems; interval time-varying delay; delay-dependent; 2-D Jensen inequalities; state feedback

### 0 引言

二维(2-D)系统是依赖于两个无关状态(水平和垂直)变化的动态过程. 2-D 离散系统广泛存在于现代工程领域, 如轧机系统、气体吸收和空气干燥过程<sup>[1]</sup>, 此外, 在数字滤波、图像增强、信号处理和其他领域也有广泛应用<sup>[2]</sup>. 广泛的应用背景使得 2-D 离散系统的稳定性分析、控制综合和滤波设计问题成为国内外众多学者的研究热点<sup>[3-8]</sup>. 许多 2-D 系统中时滞是不可避免的, 如有限的放大器转换速度或有限的信号传播时间. 时滞的存在通常是造成系统不稳定和破坏系统性能的根源, 因此, 对 2-D 时滞系统的研究具有重要的实际意义. 2-D 时滞系统的早期研究主要利用时滞无关方法<sup>[9-11]</sup>. 由于时滞相关方法考虑

了时延的长度, 比时滞无关方法具有更小的保守性, 特别是在时滞较小时, 从而 2-D 离散系统的时滞相关稳定与控制问题受到越来越多的重视<sup>[12-15]</sup>. 进一步, 考虑到时变时滞情形广泛存在于工程领域<sup>[16]</sup>, 通过 Lyapunov 方法分析其稳定性已成为研究热点. 文献 [17] 提出了系统的时滞相关稳定性准则和改进的锥补线性化算法以实现其状态反馈控制. 文献 [18] 考虑了 Roesser 模型描述的 2-D 正实系统的稳定问题. 特别是针对区间时变时滞(时滞项下界大于 0)情形, 文献 [19] 研究了 2-D 马尔可夫跳跃系统的时滞相关滤波问题. 文献 [20] 充分考虑了非线性 2-D 区间时变时滞系统的稳定性问题. 文献 [21] 针对离散 2-D FMLSS 模型, 分析其时滞相关稳定性和静态输出反馈控制问

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题. 文献[22]通过状态反馈实现了系统的稳定控制.

以上关于 2-D 时变系统的研究成果大多是利用时滞相关方法, 引入松弛变量或自由加权矩阵, 分析系统的稳定性和控制器设计问题. 对于时变时滞系统, 这一方法在对 Lyapunov 函数差分没有忽略任意有用项, 使时变项和其上界及差分项都被考虑, 从而得到保守性更小的时滞相关稳定性准则<sup>[17]</sup>. 然而, 稳定性准则含有大量的松弛矩阵或自由加权矩阵, 会导致沉重的运算负担和更复杂的综合过程, 特别是对 2-D 系统, 为了减轻运算负担, 结合 1-D 离散 Jensen 不等式方法<sup>[23-25]</sup>, 文献[19]首次将 Jensen 不等式引入 Lyapunov 函数差分, 但差分对系数互为倒数的两个正定矩阵利用不等式估计其下界, 两次不等式的应用会使得结果保守性增强.

鉴于此, 本文对具有区间时变时滞 2-D 离散系统的稳定和控制问题进行研究. 选取具有时变时滞上下界的 Lyapunov 函数, 差分考虑所有项并只引入 2-D Jensen 不等式, 舍弃权值调整方法, 得到系统的时滞相关稳定条件. 所得条件含有更少的待定矩阵, 从而在保证系统稳定性的同时减轻了运算负担. 应用上述条件, 通过状态反馈实现系统稳定控制, 保证系统稳定的条件和反馈增益矩阵的求解方法均由 LMI 给出. 最后, 通过数值算例验证了所得结果的有效性.

## 1 问题描述

考虑具有区间状态滞后的 2-D 离散系统

$$\begin{aligned} x(i+1, j+1) = & \\ A_1 x(i+1, j) + A_2 x(i, j+1) + & \\ A_{1d} x(i+1, j-d_1(j)) + A_{2d} x(i-d_2(i), j+1). \end{aligned} \quad (1)$$

其中:  $x(i, j) \in R^n$  为状态向量;  $A_k, A_{kd} (k=1, 2)$  为具有相应维数的常数矩阵;  $d_1(j), d_2(i)$  分别为水平和垂直方向的时变滞后项, 满足

$$0 < d_{1m} \leq d_1(j) \leq d_{1M}, \quad 0 < d_{2m} \leq d_2(i) \leq d_{2M}. \quad (2)$$

假设系统(1)的边界条件为

$$\begin{aligned} \{x(i, j) = \varphi_{i,j}\}, \quad \forall i \geq 0, j = -d_{1M}, -d_{1M} + 1, \dots, 0; \\ \{x(i, j) = \psi_{i,j}\}, \quad \forall j \geq 0, i = -d_{2M}, -d_{2M} + 1, \dots, 0, \\ \varphi_{0,0} = \psi_{0,0}, \end{aligned} \quad (3)$$

其中函数  $\varphi_{i,j}$  和  $\psi_{i,j}$  满足

$$\sum_{i=0}^{\infty} \sum_{j=-d_1}^0 \varphi_{i,j}^T \varphi_{i,j} < \infty, \quad \sum_{j=0}^{\infty} \sum_{i=-d_2}^0 \psi_{i,j}^T \psi_{i,j} < \infty.$$

**注 1** 不失一般性, 假设  $d_{km} < d_{kM} (k=1, 2)$ . 事实上, 当  $d_{km} = d_{kM} (k=1, 2)$  时, 由式(2)可得  $d_1(j)$  和  $d_2(i)$  是常量, 系统(1)变为具有常时滞的离散系统, 利用状态变换方法可转化为自由延迟系统.

**引理 1** 对于任意定常矩阵  $W \in R^{m \times m}$ , 其中  $W = W^T > 0$ , 整数  $l_1 < l_2$ , 向量函数  $\omega : \{l_1, l_1 + 1,$

$\dots, l_2\} \rightarrow R^m$ , 有

$$\begin{aligned} (l_2 - l_1 + 1) \sum_{i=l_1}^{l_2} \omega^T(i, j) W \omega(i, j) \geq \\ \left( \sum_{i=l_1}^{l_2} \omega(i, j) \right)^T W \left( \sum_{i=l_1}^{l_2} \omega(i, j) \right), \end{aligned} \quad (4)$$

$$\begin{aligned} (l_2 - l_1 + 1) \sum_{j=l_1}^{l_2} \omega^T(i, j) W \omega(i, j) \geq \\ \left( \sum_{j=l_1}^{l_2} \omega(i, j) \right)^T W \left( \sum_{j=l_1}^{l_2} \omega(i, j) \right). \end{aligned} \quad (5)$$

不等式(4)和(5)可称为 2-D Jensen 不等式.

**证明** 由文献[23]中引理 3 的证明可见, 固定  $j$ , 对于任意的  $l_1 \leq i \leq l_2$ , 或固定  $i$ , 对于任意的  $l_1 \leq j \leq l_2$ , 利用 Schur 补性质可以得到

$$\begin{bmatrix} \omega^T(i, j) W \omega(i, j) & \omega^T(i, j) \\ \omega(i, j) & W^{-1} \end{bmatrix} \geq 0.$$

固定  $j$ , 对于任意的  $l_1 \leq i \leq l_2$ , 将上式求和得

$$\begin{bmatrix} \sum_{i=l_1}^{l_2} \omega^T(i, j) W \omega(i, j) & \sum_{i=l_1}^{l_2} \omega^T(i, j) \\ \sum_{i=l_1}^{l_2} \omega(i, j) & (l_2 - l_1 + 1) W^{-1} \end{bmatrix} \geq 0,$$

进而固定  $i$ , 对于任意的  $l_1 \leq j \leq l_2$ , 求和得

$$\begin{bmatrix} \sum_{j=l_1}^{l_2} \omega^T(i, j) W \omega(i, j) & \sum_{j=l_1}^{l_2} \omega^T(i, j) \\ \sum_{j=l_1}^{l_2} \omega(i, j) & (l_2 - l_1 + 1) W^{-1} \end{bmatrix} \geq 0.$$

再次应用 Schur 补性质得到不等式(4)和(5)成立.  $\square$

可将引理 1 可看作是 1-D 离散 Jensen 不等式<sup>[23]</sup>的推广, 这对于本文主要结果的获得是非常必要的.

## 2 时滞相关稳定性准则

本节研究系统(1)的时滞相关稳定问题, 由 LMI 给出含有更少待定矩阵的稳定性准则.

**定理 1** 给定  $d_{km}$  和  $d_{kM} (0 < d_{km} < d_{kM}, k=1, 2)$ , 对于具有边界条件(3), 且时滞项  $d_1(j)$  和  $d_2(i)$  满足式(2)的 2-D 系统(1), 如果存在  $P > 0, Q > 0, R_k > 0, Q_k > 0, S_k > 0, Z_k > 0 (k=1, 2), X$  和  $Y$  使得

$$\begin{bmatrix} -Z_1 & 0 & X & 0 \\ * & \Psi_1 & 0 & \Phi^T \\ * & * & -Z_1 & 0 \\ * & * & * & \Psi_2 \end{bmatrix} < 0, \quad (6)$$

$$\begin{bmatrix} -Z_2 & 0 & Y & 0 \\ * & \Psi_1 & 0 & \Phi^T \\ * & * & -Z_2 & 0 \\ * & * & * & \Psi_2 \end{bmatrix} < 0 \quad (7)$$

成立. 其中

$$\Psi_1 = \begin{bmatrix} -\bar{Q} + R + \hat{Q} - \bar{S} & 0 & \bar{S} & 0 \\ * & -\tilde{Q} & 0 & 0 \\ * & * & -\bar{S} & 0 \\ * & * & * & -R \end{bmatrix},$$

$$\bar{Q} = \text{diag}\{P, P - Q\}, R = \text{diag}\{R_1, R_2\},$$

$$\bar{S} = \text{diag}\{S_1, S_2\}, \tilde{Q} = \text{diag}\{Q_1, Q_2\},$$

$$\hat{Q} = \text{diag}\{(d_{12} + 1)Q_1, (d_{21} + 1)Q_2\}, l = 1, 2,$$

$$\Phi^T = [\Phi_1^T, d_{1m}^2 \Phi_{21}^T, d_{12}^2 \Phi_{21}^T, d_{2m}^2 \Phi_{22}^T, d_{21}^2 \Phi_{22}^T],$$

$$d_{12} = d_{1M} - d_{1m}, d_{21} = d_{2M} - d_{2m},$$

$$\Phi_1 = [A_1 \ A_2 \ A_{1d} \ A_{2d} \ 0 \ 0 \ 0 \ 0],$$

$$\Psi_2 = -\text{diag}\{P, d_{1m}^2 S_1, d_{12}^2 Z_1, d_{2m}^2 S_2, d_{21}^2 Z_2\},$$

$$\Phi_{21} = [A_1 - I \ A_2 \ A_{1d} \ A_{2d} \ 0 \ 0 \ 0 \ 0],$$

$$\Phi_{22} = [A_1 \ A_2 - I \ A_{1d} \ A_{2d} \ 0 \ 0 \ 0 \ 0].$$

则系统 (1) 是渐近稳定的.

证明 记

$$x_{\xi, \eta} = x(i + \xi, j + \eta),$$

$$\bar{y}_{l,1} = x_{1,l+1} - x_{1,l}, \bar{y}_{l,1} = x_{l+1,1} - x_{l,1}. \quad (8)$$

选取 Lyapunov 函数

$$V_{11} = V_{11}^{(1)} + V_{11}^{(2)} + V_{11}^{(3)} + V_{11}^{(4)} + V_{11}^{(5)}. \quad (9)$$

其中

$$V_{11}^{(1)} = x_{1,1}^T P x_{1,1},$$

$$V_{11}^{(2)} = \sum_{l=-d_{1M}}^{-1} x_{1,l+1}^T R_1 x_{1,l+1} + \sum_{l=-d_{2M}}^{-1} x_{l+1,1}^T R_2 x_{l+1,1},$$

$$V_{11}^{(3)} = \sum_{\theta=-d_{1M}}^{-d_{1m}} \sum_{l=\theta}^{-1} x_{1,l+1}^T Q_1 x_{1,l+1} + \sum_{\theta=-d_{2M}}^{-d_{2m}} \sum_{l=\theta}^{-1} x_{l+1,1}^T Q_2 x_{l+1,1},$$

$$V_{11}^{(4)} = d_{1m} \sum_{\theta=-d_{1m}}^{-1} \sum_{l=\theta}^{-1} \bar{y}_{1,l+1}^T S_1 \bar{y}_{1,l+1} + d_{2m} \sum_{\theta=-d_{2m}}^{-1} \sum_{l=\theta}^{-1} \bar{y}_{l+1,1}^T S_2 \bar{y}_{l+1,1},$$

$$V_{11}^{(5)} = d_{12} \sum_{\theta=-d_{1M}}^{-d_{1m}-1} \sum_{l=\theta}^{-1} \bar{y}_{1,l+1}^T Z_1 \bar{y}_{1,l+1} + d_{21} \sum_{\theta=-d_{2M}}^{-d_{2m}-1} \sum_{l=\theta}^{-1} \bar{y}_{l+1,1}^T Z_2 \bar{y}_{l+1,1},$$

$P > 0, Q > 0, R_{kl} > 0, Q_k > 0, S_k > 0$  和  $Z_k > 0 (k, l = 1, 2)$  是具有相应维数的常数矩阵.

定义 Lyapunov 函数 (9) 的差分为

$$\Delta V = V_{11} - V_{d1} - V_{d2}.$$

其中

$$V_{d1} = V_{d1}^{(1)} + V_{d1}^{(2)} + V_{d1}^{(3)} + V_{d1}^{(4)} + V_{d1}^{(5)},$$

$$V_{d1}^{(1)} = x_{1,0}^T Q x_{1,0}, V_{d1}^{(2)} = \sum_{l=-d_{1M}}^{-1} x_{1,l}^T R_1 x_{1,l},$$

$$V_{d1}^{(3)} = \sum_{\theta=-d_{1M}}^{-d_{1m}} \sum_{l=\theta}^{-1} x_{1,l}^T Q_1 x_{1,l},$$

$$V_{d1}^{(4)} = d_{1m} \sum_{\theta=-d_{1m}}^{-1} \sum_{l=\theta}^{-1} \bar{y}_{1,l}^T S_1 \bar{y}_{1,l},$$

$$V_{d1}^{(5)} = d_{12} \sum_{\theta=-d_{1M}}^{-d_{1m}-1} \sum_{l=\theta}^{-1} \bar{y}_{1,l}^T Z_1 \bar{y}_{1,l},$$

$$V_{d2} = V_{d2}^{(1)} + V_{d2}^{(2)} + V_{d2}^{(3)} + V_{d2}^{(4)} + V_{d2}^{(5)},$$

$$V_{d2}^{(1)} = x_{0,1}^T (P - Q) x_{0,1}, V_{d2}^{(2)} = \sum_{l=-d_{2M}}^{-1} x_{l,1}^T R_2 x_{l,1},$$

$$V_{d2}^{(3)} = \sum_{\theta=-d_{2M}}^{-d_{2m}} \sum_{l=\theta}^{-1} x_{l,1}^T Q_2 x_{l,1},$$

$$V_{d2}^{(4)} = d_{2m} \sum_{\theta=-d_{2m}}^{-1} \sum_{l=\theta}^{-1} \bar{y}_{l,1}^T S_2 \bar{y}_{l,1},$$

$$V_{d2}^{(5)} = d_{21} \sum_{\theta=-d_{2M}}^{-d_{2m}-1} \sum_{l=\theta}^{-1} \bar{y}_{l,1}^T Z_2 \bar{y}_{l,1}.$$

进而得到

$$\Delta V = \Delta V^{(1)} + \Delta V^{(2)} + \Delta V^{(3)} + \Delta V^{(4)} + \Delta V^{(5)}. \quad (10)$$

其中

$$\Delta V^{(1)} = V_{11}^{(1)} - V_{d1}^{(1)} - V_{d2}^{(1)} = \xi_1^T \Phi_1^T P \Phi_1 \xi_1 - x^T \tilde{Q} x,$$

$$x = [x_{1,0}^T \ x_{0,1}^T]^T, x_d = [x_{1,-d_1(j)}^T \ x_{-d_2(i)}^T],$$

$$x_{dM} = [x_{1,-d_{1M}}^T \ x_{-d_{2M},1}^T]^T,$$

$$\Delta V^{(2)} = V_{11}^{(2)} - V_{d1}^{(2)} - V_{d2}^{(2)} = x^T R x - x_{dM}^T R x_{dM},$$

$$\Delta V^{(3)} = V_{11}^{(3)} - V_{d1}^{(3)} - V_{d2}^{(3)} =$$

$$x^T \hat{Q} x - \sum_{l=-d_{1M}}^{-d_{1m}} x_{1,l}^T Q_1 x_{1,l} - \sum_{l=-d_{2M}}^{-d_{2m}} x_{l,1}^T Q_2 x_{l,1} \leq$$

$$x^T \hat{Q} x - x_d^T \tilde{Q} x_d,$$

$$\Delta V^{(4)} = V_{11}^{(4)} - V_{d1}^{(4)} - V_{d2}^{(4)} =$$

$$d_{1m}^2 \bar{y}_{1,0}^T S_1 \bar{y}_{1,0} + d_{2m}^2 \bar{y}_{0,1}^T S_2 \bar{y}_{0,1} -$$

$$d_{1m} \sum_{l=-d_{1m}}^{-1} \bar{y}_{1,l}^T S_1 \bar{y}_{1,l} - d_{2m} \sum_{l=-d_{2m}}^{-1} \bar{y}_{l,1}^T S_2 \bar{y}_{l,1},$$

$$\Delta V^{(5)} = V_{11}^{(5)} - V_{d1}^{(5)} - V_{d2}^{(5)} =$$

$$d_{12}^2 \bar{y}_{1,0}^T Z_1 \bar{y}_{1,0} + d_{21}^2 \bar{y}_{0,1}^T Z_2 \bar{y}_{0,1} -$$

$$d_{12} \sum_{l=-d_{1M}}^{-d_{1m}-1} \bar{y}_{1,l}^T Z_1 \bar{y}_{1,l} - d_{21} \sum_{l=-d_{2M}}^{-d_{2m}-1} \bar{y}_{l,1}^T Z_2 \bar{y}_{l,1}.$$

利用 2-D Jensen 不等式 (4) 和 (5), 可以得到

$$-d_{1m} \sum_{l=-d_{1m}}^{-1} \bar{y}_{1,l}^T S_1 \bar{y}_{1,l} \leq$$

$$\begin{aligned}
 & - \left( \sum_{l=-d_{1m}}^{-1} \bar{y}_{1,l} \right)^T S_1 \left( \sum_{l=-d_{1m}}^{-1} \bar{y}_{1,l} \right) = \\
 & - (x_{1,0} - x_{1,-d_{1m}})^T S_1 (x_{1,0} - x_{1,-d_{1m}}), \quad (11) \\
 & - d_{2m} \sum_{l=-d_{2m}}^{-1} \bar{y}_{l,1}^T S_2 \bar{y}_{l,1} \leq \\
 & - \left( \sum_{l=-d_{2m}}^{-1} \bar{y}_{l,1} \right)^T S_2 \left( \sum_{l=-d_{2m}}^{-1} \bar{y}_{l,1} \right) = \\
 & - (x_{0,1} - x_{-d_{2m},1})^T S_2 (x_{0,1} - x_{-d_{2m},1}). \quad (12)
 \end{aligned}$$

结合式(10)有

$$\begin{aligned}
 \Delta V \leq & \frac{1}{d_{12}} \sum_{l=-d_{1M}}^{-d_1(j)-1} \begin{bmatrix} \xi_1 \\ -d_{12} \bar{y}_{1,l} \end{bmatrix}^T \begin{bmatrix} \Psi & 0 \\ 0 & -Z_1 \end{bmatrix} \begin{bmatrix} \xi_1 \\ -d_{12} \bar{y}_{1,l} \end{bmatrix} + \\
 & \frac{1}{d_{12}} \sum_{l=-d_1(j)}^{-d_{1m}-1} \begin{bmatrix} \xi_1 \\ -d_{12} \bar{y}_{1,l} \end{bmatrix}^T \begin{bmatrix} \Psi & 0 \\ 0 & -Z_1 \end{bmatrix} \begin{bmatrix} \xi_1 \\ -d_{12} \bar{y}_{1,l} \end{bmatrix} + \\
 & \frac{1}{d_{21}} \sum_{l=-d_{2M}}^{-d_2(i)-1} \begin{bmatrix} \xi_1 \\ -d_{21} \bar{y}_{l,1} \end{bmatrix}^T \begin{bmatrix} \Psi & 0 \\ 0 & -Z_2 \end{bmatrix} \begin{bmatrix} \xi_1 \\ -d_{21} \bar{y}_{l,1} \end{bmatrix} + \\
 & \frac{1}{d_{21}} \sum_{l=-d_2(i)}^{-d_{2m}-1} \begin{bmatrix} \xi_1 \\ -d_{21} \bar{y}_{l,1} \end{bmatrix}^T \begin{bmatrix} \Psi & 0 \\ 0 & -Z_2 \end{bmatrix} \begin{bmatrix} \xi_1 \\ -d_{21} \bar{y}_{l,1} \end{bmatrix}. \quad (13)
 \end{aligned}$$

其中

$$\begin{aligned}
 \xi_1 = & [x_{1,0}^T, x_{0,1}^T, x_{1,-d_1(j)}^T, x_{-d_2(i),1}^T, x_{1,-d_{1m}}^T, \\
 & x_{-d_{2m},1}^T, x_{1,-d_{1M}}^T, x_{-d_{2M},1}^T]^T, \\
 \Psi = & \Psi_1 + \Phi_1^T P \Phi_1 + \Phi_{21}^T (d_{1m}^2 S_1 + d_{12}^2 Z_1) \Phi_{21} + \\
 & \Phi_{22}^T (d_{2m}^2 S_2 + d_{21}^2 Z_2) \Phi_{22}.
 \end{aligned}$$

文献[26]的引理4.1表明,存在具有相应维数的矩阵  $X$  和  $Y$  分别满足

$$\begin{bmatrix} -Z_1 & 0 & X \\ * & \Psi & 0 \\ * & * & -Z_1 \end{bmatrix} < 0, \quad \begin{bmatrix} -Z_2 & 0 & Y \\ * & \Psi & 0 \\ * & * & -Z_2 \end{bmatrix} < 0, \quad (14)$$

当且仅当

$$\begin{bmatrix} \Psi & 0 \\ 0 & -Z_1 \end{bmatrix} < 0, \quad \begin{bmatrix} \Psi & 0 \\ 0 & -Z_2 \end{bmatrix} < 0.$$

结合式(13),对于所有非零  $\xi_1$ ,有  $\Delta V < 0$ ,当且仅当式(14)成立.利用Schur补性质,LMI(6)和(7)等价于式(14),即如果LMI(6)和(7)成立,则  $\Delta V < 0$ ,系统(1)是渐近稳定的.□

**注2** 定理1的证明中,在计算  $\Delta V$  时,  $d_{1M}$  和  $d_{2M}$  都分成了  $d_{1M} = d_1(j) + (d_{1M} - d_1(j))$  和  $d_{2M} = d_2(i) + (d_{2M} - d_2(i))$  两部分,使得和式计算结果没有任何增加,从而得到具有更小保守性的稳定性准则.

**注3** 在Lyapunov函数(9)中选取  $V_{11}^{(4)}$  和  $V_{11}^{(5)}$ ,对其差分时结合2-D Jensen不等式(4)和(5)得到式

(11)和(12),进而给出系统(1)基于LMI(6)和(7)的新的时滞相关稳定性准则.2-D Jensen不等式的应用避免了已有自由加权矩阵法对过多待定矩阵的引入,使LMI(6)和(7)比2-D时变时滞系统已有的稳定性成果含有更少的待定矩阵,从而降低了沉重的运算负担.

### 3 状态反馈控制器设计

本节研究具有控制输入的2-D系统(1)的控制问题.基于前文的稳定性分析,利用时滞相关方法,设计状态反馈控制器保证系统稳定.考虑具有控制输入的2-D系统(1),有

$$\begin{aligned}
 x(i+1, j+1) = & A_1 x(i+1, j) + A_2 x(i, j+1) + \\
 & A_{1d} x(i+1, j-d_1(j)) + A_{2d} x(i-d_2(i), j+1) + \\
 & B_1 u(i+1, j) + B_2 u(i, j+1). \quad (15)
 \end{aligned}$$

其中:  $u(i, j) \in R^p$  为控制输入;  $B_k (k=1, 2)$  为具有相应维数的常矩阵;时变滞后  $d_1(j), d_2(i)$  和边界条件与式(2)和(3)形式相同.

设计2-D状态反馈控制器

$$u(i, j) = Kx(i, j). \quad (16)$$

将式(16)代入2-D系统(15)可得闭环系统

$$\begin{aligned}
 x(i+1, j+1) = & (A_1 + B_1 K)x(i+1, j) + (A_2 + B_2 K)x(i, j+1) + \\
 & A_{1d} x(i+1, j-d_1(j)) + A_{2d} x(i-d_2(i), j+1). \quad (17)
 \end{aligned}$$

**定理2** 给定  $t_k, t_{k+2}, d_{km}$  和  $d_{kM} (0 < d_{km} < d_{kM}, k=1, 2)$ ,对于具有边界条件(3)和时滞项满足式(2)的2-D系统(15),如果存在  $\tilde{P} > 0, \tilde{Q} > 0, \tilde{R}_k > 0, \tilde{Q}_k > 0, \tilde{S}_k > 0, \tilde{Z}_k > 0, k=1, 2, \tilde{X}, \tilde{Y}$  和  $V$ ,使得

$$\begin{bmatrix} -\tilde{Z}_1 & 0 & \tilde{X} & 0 \\ * & \tilde{\Psi}_1 & 0 & \tilde{\Phi}^T \\ * & * & -\tilde{Z}_1 & 0 \\ * & * & * & \tilde{\Psi}_2 \end{bmatrix} < 0, \quad (18)$$

$$\begin{bmatrix} -\tilde{Z}_2 & 0 & \tilde{Y} & 0 \\ * & \tilde{\Psi}_1 & 0 & \tilde{\Phi}^T \\ * & * & -\tilde{Z}_2 & 0 \\ * & * & * & \tilde{\Psi}_2 \end{bmatrix} < 0 \quad (19)$$

成立.其中

$$\tilde{\Psi}_1 = \begin{bmatrix} -\bar{Q}_1 + \tilde{R} + \hat{Q}_1 - \tilde{S} & 0 & \bar{S} & 0 \\ * & -\tilde{Q}_{12} & 0 & 0 \\ * & * & -\tilde{S} & 0 \\ * & * & * & -\tilde{R} \end{bmatrix},$$

$$\bar{Q}_1 = \text{diag}\{\tilde{P}, \tilde{P} - \tilde{Q}\}, \tilde{R} = \text{diag}\{\tilde{R}_1, \tilde{R}_2\},$$

$$\hat{Q}_1 = \text{diag}\{(d_{12} + 1)\tilde{Q}_1, (d_{21} + 1)\tilde{Q}_2\},$$

$$\tilde{S} = \text{diag}\{\tilde{S}_1, \tilde{S}_2\}, \tilde{Q}_{12} = \text{diag}\{\tilde{Q}_1, \tilde{Q}_2\},$$

$$\begin{aligned} \tilde{\Phi}^T &= [\tilde{\Phi}_1^T \ t_1 d_{1m}^2 \tilde{\Phi}_{21}^T \ t_3 d_{12}^2 \tilde{\Phi}_{21}^T \ t_2 d_{2m}^2 \tilde{\Phi}_{22}^T \ t_4 d_{21}^2 \tilde{\Phi}_{22}^T], \\ \tilde{\Phi}_1 &= [A_1 \tilde{P} + B_1 V \ A_2 \tilde{P} + B_2 V \ A_{1d} \tilde{P} \ A_{2d} \tilde{P} \ 0 \ 0 \ 0 \ 0], \\ \tilde{\Phi}_{21} &= [(A_1 - I) \tilde{P} + B_1 V \ A_2 \tilde{P} + B_2 V \ \rightarrow \\ &\quad \leftarrow A_{1d} \tilde{P} \ A_{2d} \tilde{P} \ 0 \ 0 \ 0 \ 0], \\ \tilde{\Phi}_{22} &= [A_1 \tilde{P} + B_1 V \ (A_2 - I) \tilde{P} + B_2 V \ \rightarrow \\ &\quad \leftarrow A_{1d} \tilde{P} \ A_{2d} \tilde{P} \ 0 \ 0 \ 0 \ 0], \\ \tilde{\Psi}_2 &= -\text{diag}\{\tilde{P}, t_1 d_{1m}^2 \tilde{P}, t_3 d_{12}^2 \tilde{P}, t_2 d_{2m}^2 \tilde{P}, t_4 d_{21}^2 \tilde{P}\}, \\ V &= K \tilde{P}. \end{aligned} \tag{20}$$

则控制器(16)保证系统(15)稳定.

**证明** 将定理1应用于闭环系统(17), 用  $A_k + B_k K$  替换 LMI(6)和(7)中的  $A_k$  ( $k = 1, 2$ ), 得到保证闭环系统(17)稳定的新 LMI. 令

$$\begin{aligned} S_k &= t_k P, \ Z_k = t_{k+2} P, \ \tilde{P} = P^{-1}, \ \tilde{Q} = \tilde{P} Q \tilde{P}, \\ \tilde{R}_k &= \tilde{P} R_k \tilde{P}, \ \tilde{Q}_k = \tilde{P} Q_k \tilde{P}, \ \tilde{S}_k = \tilde{P} S_k \tilde{P}, \\ \tilde{Z}_k &= \tilde{P} Z_k \tilde{P}, \ \tilde{X} = \tilde{P} X \tilde{P}, \ \tilde{Y} = \tilde{P} Y \tilde{P}, \ k = 1, 2. \end{aligned}$$

利用  $\text{diag}\{\tilde{P}, \tilde{P}, \tilde{P}\}$  对得到的新 LMI 作同等变换, 使得 LMI(18)和(19)成立, 即保证式(17)稳定. 由于  $\tilde{P} > 0$ , 由式(20)可解得控制器(16)为

$$u(i, j) = V \tilde{P}^{-1} x(i, j), \tag{21}$$

得到保证系统(15)稳定的控制器设计方法.  $\square$

定理2通过控制器(16)实现了系统(15)的状态反馈控制, 即保证闭环系统(17)渐近稳定.

### 4 数值算例

下面通过数值算例表明所得结果的有效性和优越性.

**例1** 考虑文献[13]的例子, 由 2-D FM LSS 模型(1)描述具有时滞的热处理过程. 考虑系统(1)的稳定性, 系统参数与文献[13]相同, 有

$$\begin{aligned} A_1 &= \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, \ A_2 = \begin{bmatrix} 0 & 0 \\ 0.25 & 0.65 \end{bmatrix}, \\ A_{1d} &= \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix}, \ A_{2d} = \begin{bmatrix} 0 & 0 \\ 0 & -0.12 \end{bmatrix}. \end{aligned} \tag{22}$$

当时滞为定常, 即  $d_1(j) = h_2$  时, 文献[13]表明, 对于任意常时滞  $h_2$ , 满足  $0 < h_2 \leq 5$ , 系统渐近稳定; 当时滞  $d_1(j)$  为时变且  $0 \leq d_1(j) \leq 13$  时, 文献[17]证明了系统的稳定性, 即  $d_1(j)$  的上界比文献[13]给出的大很多. 进而应用定理1, 对于  $1 \leq d_1(j) \leq 21$ , 系统仍渐近稳定, 即得到的稳定性准则更适用于时滞项下界大于0(时滞不可避免)的系统, 且上界比文献[17]还大.

图1为时滞项满足  $1 \leq d_1(j) \leq 21$  的系统(22)状态变量的轨迹. 很明显, 随着水平和垂直变量  $i$  和  $j$  的

逐渐增大, 系统的状态  $x(i, j)$  逐渐趋于原点0, 即系统渐近稳定.

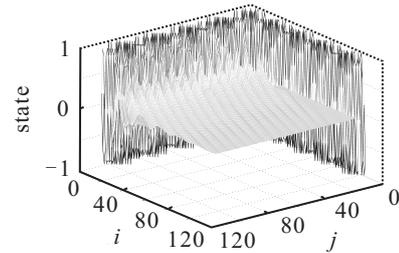


图1 时滞上界  $d_{1M}$  为 21 的系统(22)的状态轨迹

**例2** 考虑 2-D 系统(15), 系数矩阵为

$$\begin{aligned} A_1 &= \begin{bmatrix} 0.1 & 0.6 \\ 0 & 0.2 \end{bmatrix}, \ A_2 = \begin{bmatrix} 0 & 0 \\ 0.2 & 0.65 \end{bmatrix}, \ A_{1d} = 0, \\ A_{2d} &= \begin{bmatrix} 0 & 0 \\ 0 & -0.12 \end{bmatrix}, \ B_1 = \begin{bmatrix} 0.2 & 0 \\ 0.1 & 0 \end{bmatrix}, \ B_2 = \begin{bmatrix} 0.4 & 0 \\ 0.8 & 0 \end{bmatrix}. \end{aligned} \tag{23}$$

时变时滞项满足  $2 \leq d_1(j) \leq 22, 3 \leq d_2(i) \leq 18$ .

应用定理2, 给定  $t = 0.02, t_1 = 0.02, t_2 = 0.3, t_3 = 0.04, t_4 = 0.1$ , 可求解状态反馈控制问题, 即 LMI(18)和(19)的解为

$$\begin{aligned} \tilde{P} &= 10^{-10} \times \begin{bmatrix} 0.1152 & 0.0203 \\ 0.0203 & 0.0695 \end{bmatrix}, \\ V &= 10^{-10} \times \begin{bmatrix} 0.0878 & -0.1069 \\ 0 & 0 \end{bmatrix}. \end{aligned} \tag{24}$$

进而由式(21)解得状态反馈增益为

$$K = V \tilde{P}^{-1} = \begin{bmatrix} 1.0879 & -1.8545 \\ 0 & 0 \end{bmatrix}. \tag{25}$$

类似图1, 图2表明增益(25)能够保证系统(23)渐近稳定.

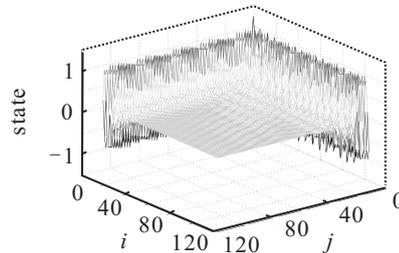


图2 具有状态反馈增益(25)的系统(23)的状态轨迹

### 5 结论

本文研究了具有区间时变状态滞后 2-D 线性离散系统的稳定和控制问题. 通过选取含有时变时滞项上、下界的新的 Lyapunov 函数, 考虑到 Lyapunov 函数差分式的所有项, 引入 Jensen 不等式, 得到基于 LMI 的稳定性准则. 该准则相比已有成果含有更少的待定矩阵, 且具有更小的保守性. 利用稳定性准则, 通过状态反馈实现了系统的稳定控制. 最后通过数值算例表明了所得结果的有效性和优越性.

## 参考文献(References)

- [1] Kaczorek T. Two-dimensional linear systems[C]. Lecture Notes in Control and Information Sciences. Berlin: Springer, 1985: 283-284.
- [2] 杨成梧, 邹云. 2-D 线性离散系统[M]. 国防工业出版社, 1995: 136-173.  
(Yang C W, Zou Y. 2-D linear discrete systems[M]. National Defense Industry Press, 1995: 136-173.)
- [3] Du C, Xie L. Stability analysis and stabilization of uncertain two-dimensional discrete systems: An LMI approach[J]. IEEE Trans on Circuits Systems, 1999, 46(11): 1371-1374.
- [4] Feng Z Y, Xu L, Wu M, et al.  $H_\infty$  static output feedback control of 2-D discrete systems in FM second model[J]. Asian J of Control, 2012, 14(6): 1505-1513.
- [5] Nima Y, Nader Y, Mariem G, et al. Lyapunov theory for 2-D nonlinear roesser models: Application to asymptotic and exponential stability[J]. IEEE Trans on Automatic Control, 2013, 58(5): 1299-1304.
- [6] Choon K A.  $l_2 - l_\infty$  elimination of overflow oscillations in 2-D digital filters described by roesser model with external interference[J]. IEEE Trans on Circuits and Systems II: Express Briefs, 2013, 60(6): 361-365.
- [7] Chen X M, Lam J, Gao H J, et al. Stability analysis and control design for 2-D fuzzy systems via basis-dependent Lyapunov functions[J]. Multidim System Signal Processing, 2013, 24(3): 395-415.
- [8] Bailo E, Gelonch J, RomeroVivo S. Advances on the reachability index of positive 2-D systems[J]. IEEE Trans on Automatic Control, 2014, 59(8): 2248-2251.
- [9] Peng D, Guan X P, Long C N. Robust output feedback guaranteed cost control for 2-D uncertain state-delayed systems[J]. Asian J of Control, 2007, 9(4): 470-474.
- [10] Xu H L, Xu S Y, Lam J. Positive real control for 2-D discrete delayed systems via output feedback controllers[J]. J of Computational and Applied Mathematics, 2008, 216(1): 87-97.
- [11] Wei Y, Qiu J, Karimi H R, et al. Filtering design for two-dimensional Markovian jump systems with state-delays and deficient mode information[J]. Information Sciences, 2014, 269(4): 316-331.
- [12] Peng D, Guan X. Output feedback control for 2-D state-delayed systems[J]. Circuits Systems Signal Process, 2009, 28(1): 147-167.
- [13] Xu J M, Yu L. Delay-dependent  $H_\infty$  control for 2-D discrete state delay systems in the second FM model[J]. Multidim System Signal Process, 2009, 20(4): 333-349.
- [14] Peng D, Guan X.  $H_\infty$  filtering of 2-D discrete state-delayed systems[J]. Multidim System Signal Process, 2009, 20(3): 265-274.
- [15] Ye S X, Li J Z. Robust control for a class of 2-D discrete uncertain delayed systems[C]. The 10th IEEE Int Conf on Control and Automation. Hangzhou, 2013: 1048-1052.
- [16] Elaydi S. An introduction to difference equations[M]. New York: Springer, 2005: 154-214.
- [17] Feng Z Y, Xu L, Wu M, et al. Delay-dependent robust stability and stabilization of uncertain 2-D discrete systems with time-varying delays[J]. IET Control Theory and Applications, 2010, 4(10): 1959-1971.
- [18] Liu X, Yu W, Wang L. Necessary and sufficient asymptotic stability criterion for 2-D positive systems with time-varying state delays described by Roesser model[J]. IET Control Theory and Applications, 2011, 5(5): 663-668.
- [19] Zhang R, Zhang Y, Hu C, et al. Delay-range-dependent filtering for two-dimensional Markovian jump systems with interval delays[J]. IET Control Theory and Applications, 2011, 5(18): 2191-2199.
- [20] 彭丹, 华长春. 具有时变状态滞后的非线性 2-D 离散系统的稳定性与控制[J]. 控制与决策, 2012, 27(1): 124-128.  
(Peng D, Hua C C. Stability and control of nonlinear 2-D discrete systems with time-varying state delays[J]. Control and Decision, 2012, 27(1): 124-128.)
- [21] Peng D, Hua C C. Delay-dependent stability and static output feedback control of 2-D discrete systems with interval time-varying delays[J]. Asian J of Control, 2014, 16(6): 1726-1734.
- [22] 彭丹, 华长春, 王春艳, 等. 具有区间时变时滞 2-D 离散系统的时滞相关稳定与控制[J]. 控制与决策, 2014, 29(6): 1041-1046.  
(Peng D, Hua C C, Wang C Y, et al. Delay-dependent stability and control of 2-D discrete systems with interval time-varying delays[J]. Control and Decision, 2014, 29(6): 1041-1046.)
- [23] Zhu X L, Yang G H. Jensen inequality approach to stability analysis of discrete-time systems with time-varying delay[C]. American Control Conf. Washington, 2008: 1644-1649.
- [24] Huang H, Feng G. Improved approach to delay-dependent stability analysis of discrete-time systems with time-varying delay[J]. IET Control Theory and Application, 2010, 4(10): 2152-2159.
- [25] Kokil P, Kar H, Kandanli V. Stability analysis of linear discrete-time systems with interval delay: A delay-partitioning approach[J]. ISRN Applied Mathematics 2011, 2011: 1-10.
- [26] Han Q L, Gu K. Stability of linear systems with time-varying delay: A generalized discretized Lyapunov functional approach[J]. Asian J of Control, 2001, 3(3): 170-180.